

Adiabatic Refractive Lenses for Making nm Sized Hard X-Ray Beams

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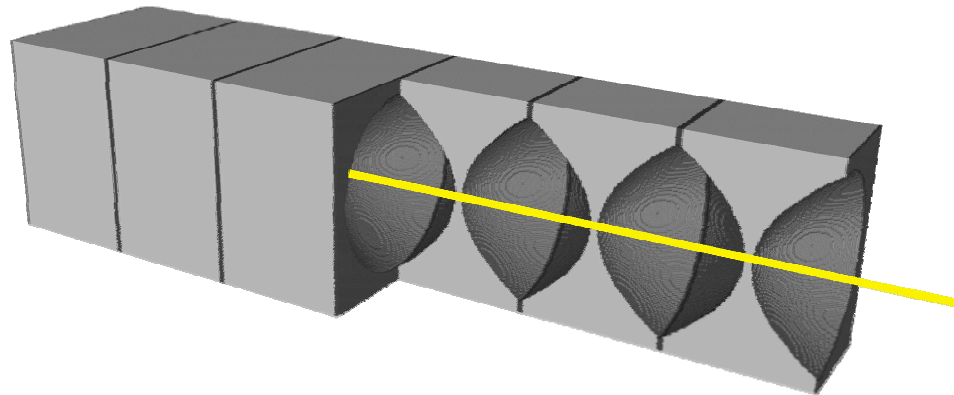
ISG, Research Center Jülich, Jülich, Germany



Refractive X-Ray Optics

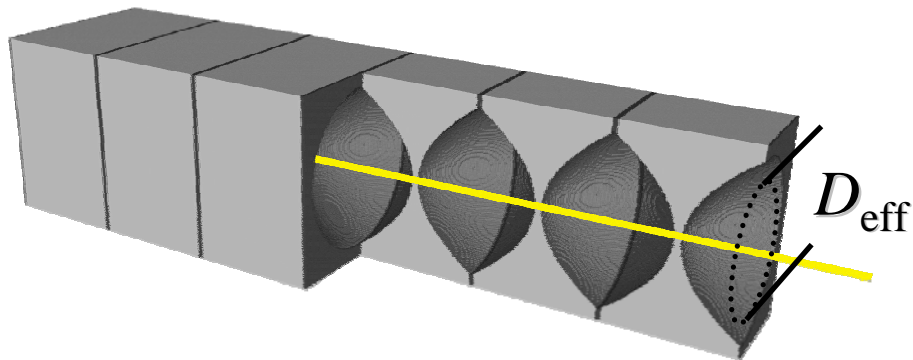
- first realized in 1996 (Snigirev et al.)
- a variety of refractive lenses have been developed since
- applied in full field imaging and scanning microscopy
- most important to achieve optimal performance:

aspherical lens shape



parabolic

Effective Aperture and Diffraction Limit

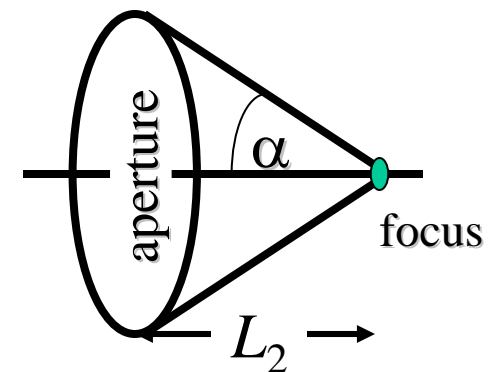


D_{eff} limited by:

- geometric aperture $2R_0$
- attenuation inside lens material (includes Compton scattering)

→ low Z lens material

Numerical aperture:



$$NA = \sin \alpha = \frac{D_{\text{eff}}}{2L_2}$$

Diffraction limit:

$$d_t = 0.75 \cdot \frac{\lambda}{2NA}$$

Numerical Aperture

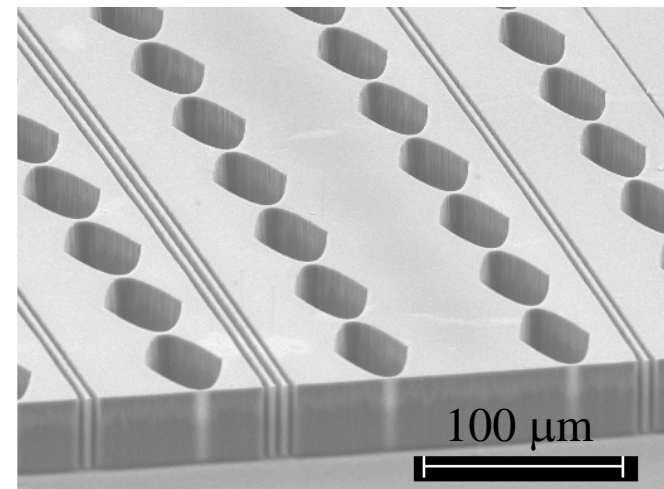
large f : aperture dominated by attenuation

$$D_{\text{eff}} = 4 \sqrt{\frac{f\delta}{\mu}} \propto \sqrt{f}$$

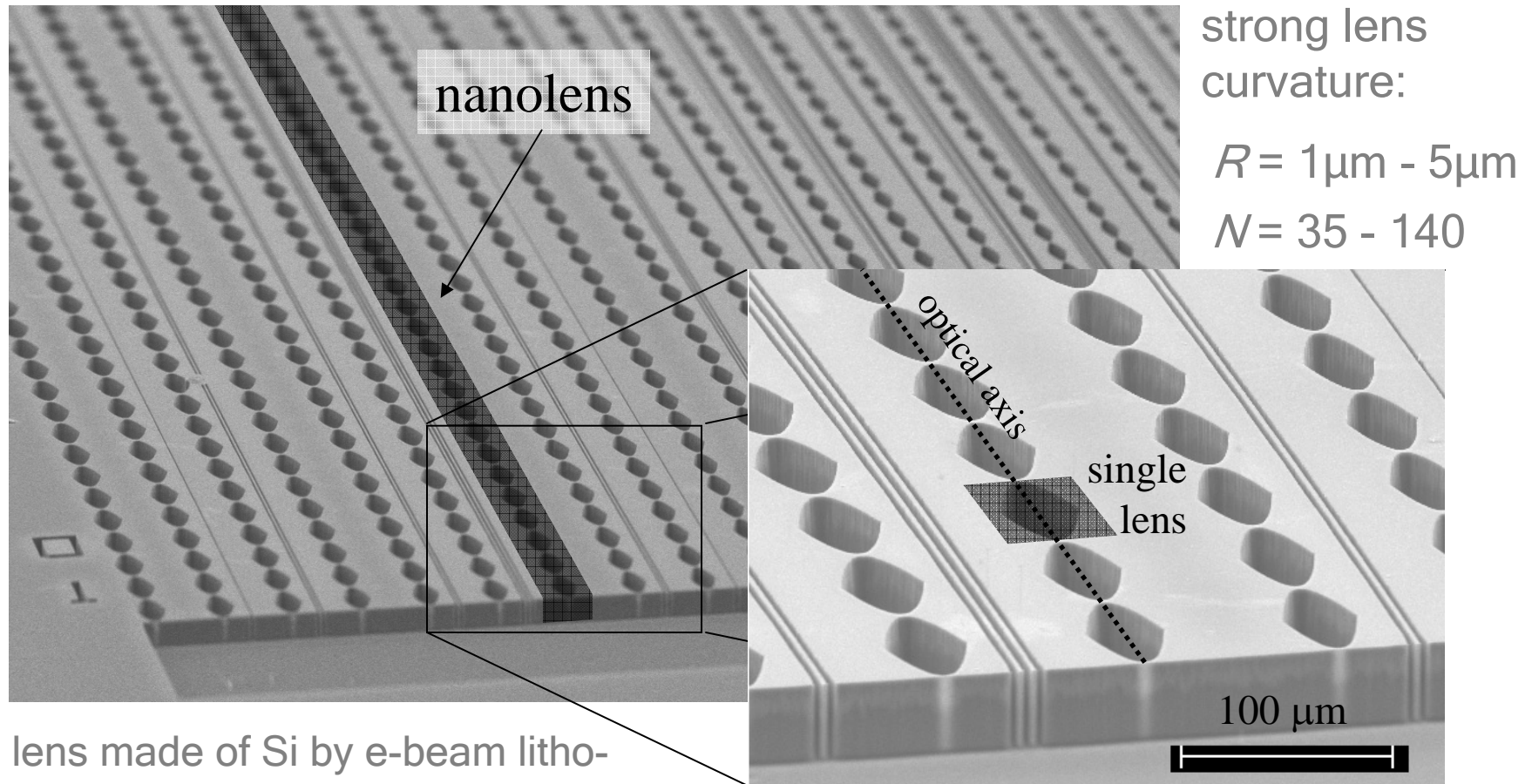
- reduce μ/δ (low Z lens material)
- $NA = D_{\text{eff}}/2f \propto 1/\sqrt{f}$: reduce focal size to minimum



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Nanofocusing Lenses (NFL)



strong lens
curvature:

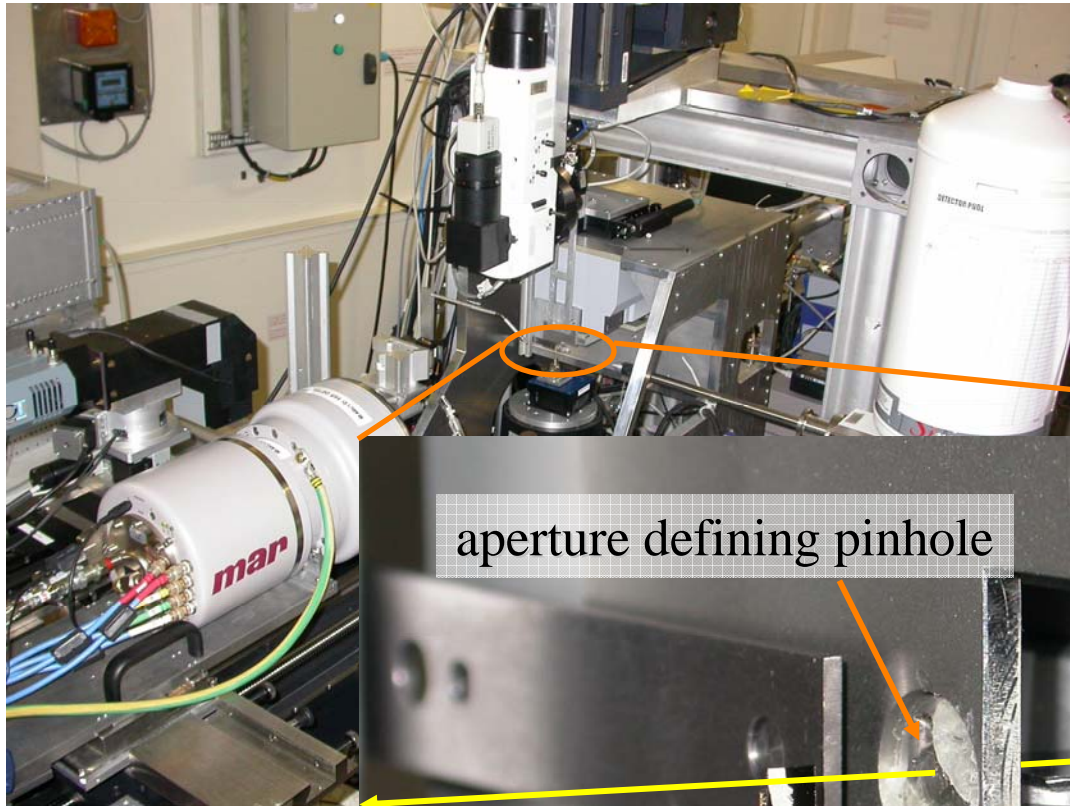
$$R = 1\mu\text{m} - 5\mu\text{m}$$

$$N = 35 - 140$$

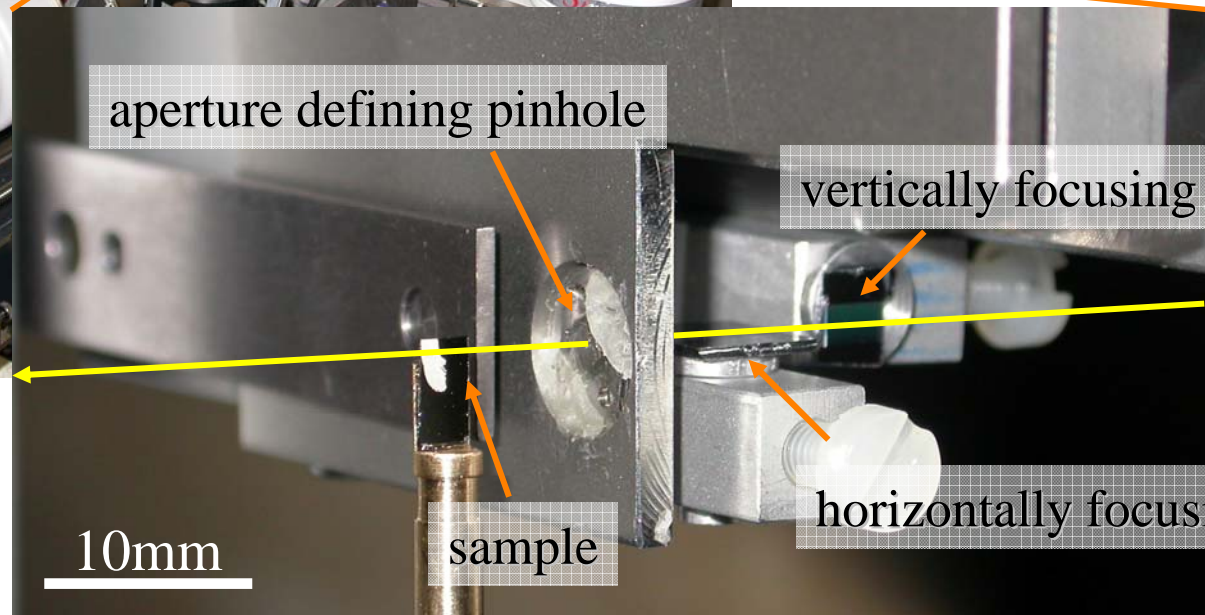
lens made of Si by e-beam litho-
graphy and deep reactive ion etching!

APL 82, 1485 (2003)

Crossed Nanofocusing Lenses



Setup at ID13
(ESRF)



Focusing with NFLs

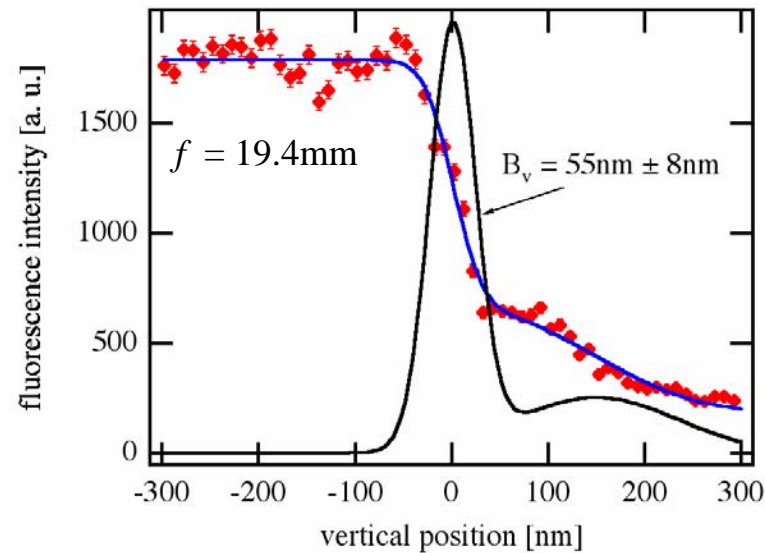
Si lens: $E = 21\text{keV}$, $L_1 = 47\text{m}$

source:

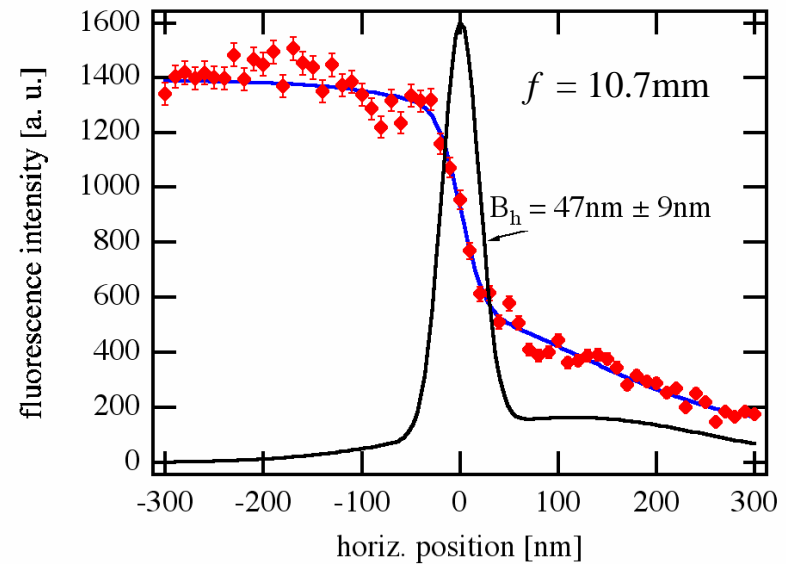
ID13 low- β invac. undulator

source size: $150 \times 60\mu\text{m}^2$

vertical focus: 55nm



horizontal focus: 47nm



demagnification:

$\sim 2400 \times 4400$

flux: $1.7 \cdot 10^8\text{ph/s}$

DOF = $42 \times 86 \mu\text{m}^2$

APL 87, 124103 (2005)

Focusing with NFLs

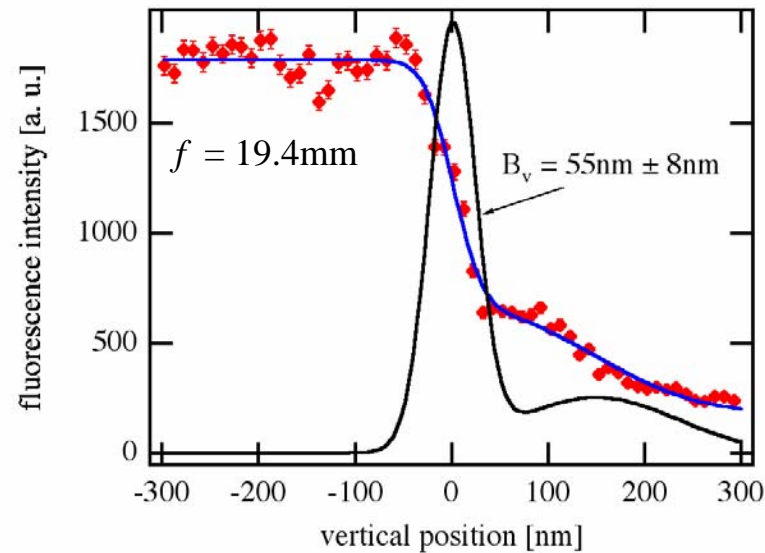
Si lens: $E = 21\text{keV}$, $L_1 = 47\text{m}$

source:

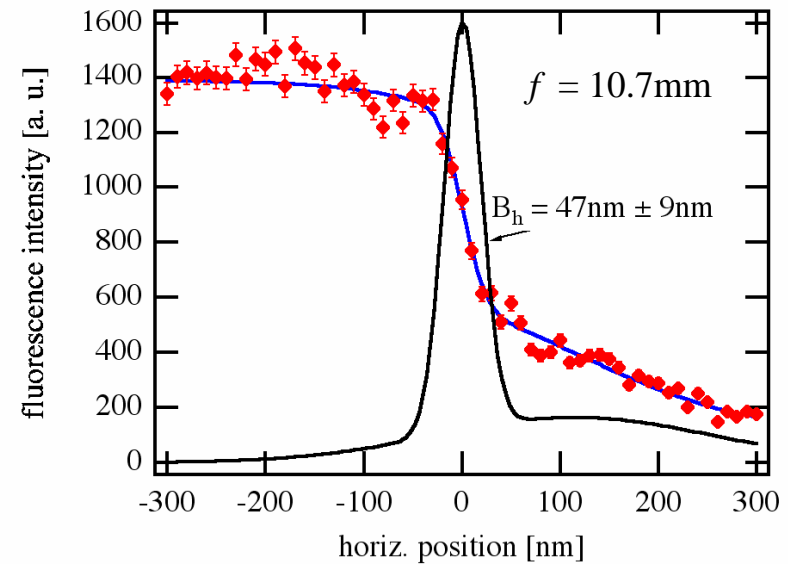
ID13 low- β invac. undulator

source size: $150 \times 60\mu\text{m}^2$

vertical focus: 55nm



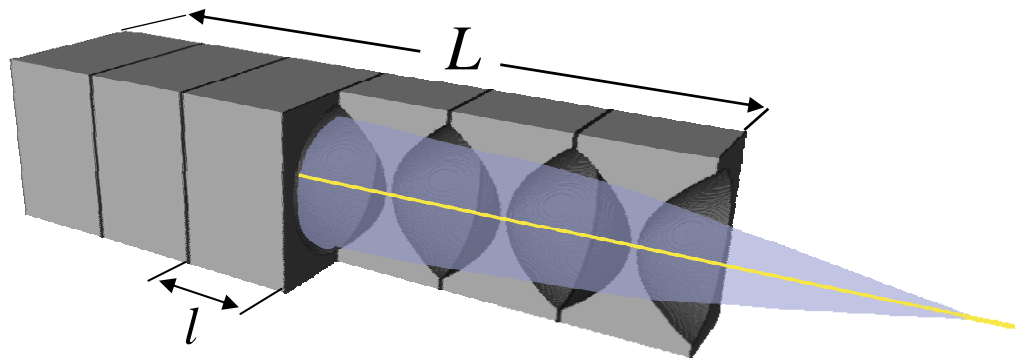
horizontal focus: 47nm



roughness: $\sim 10\text{nm rms}$

Effective Aperture and Diffraction Limit

Nanofocusing lens:



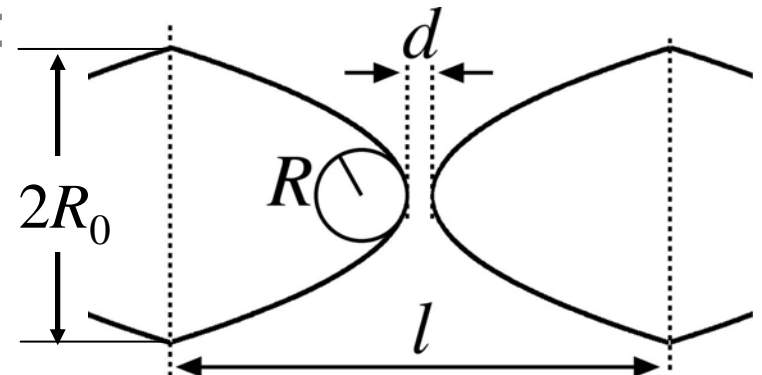
$$f_{\min} = \sqrt{f_0 L} = \sqrt{\frac{Rl}{2\delta}}$$

with $f_0 = \frac{R}{2N\delta}$

lens short (attenuation negligible):

$$D_{\text{eff}} < 2R_0 \approx 2\sqrt{Rl}$$

$$NA = \frac{D_{\text{eff}}}{2f_{\min}} \leq \frac{2\sqrt{Rl}}{2\sqrt{\frac{Rl}{2\delta}}} = \sqrt{2\delta}$$



Numerical Aperture of NFLs

$$NA = \frac{D_{\text{eff}}}{2f_{\text{min}}} \leq \sqrt{2\delta}$$

Always smaller than critical angle of total reflection

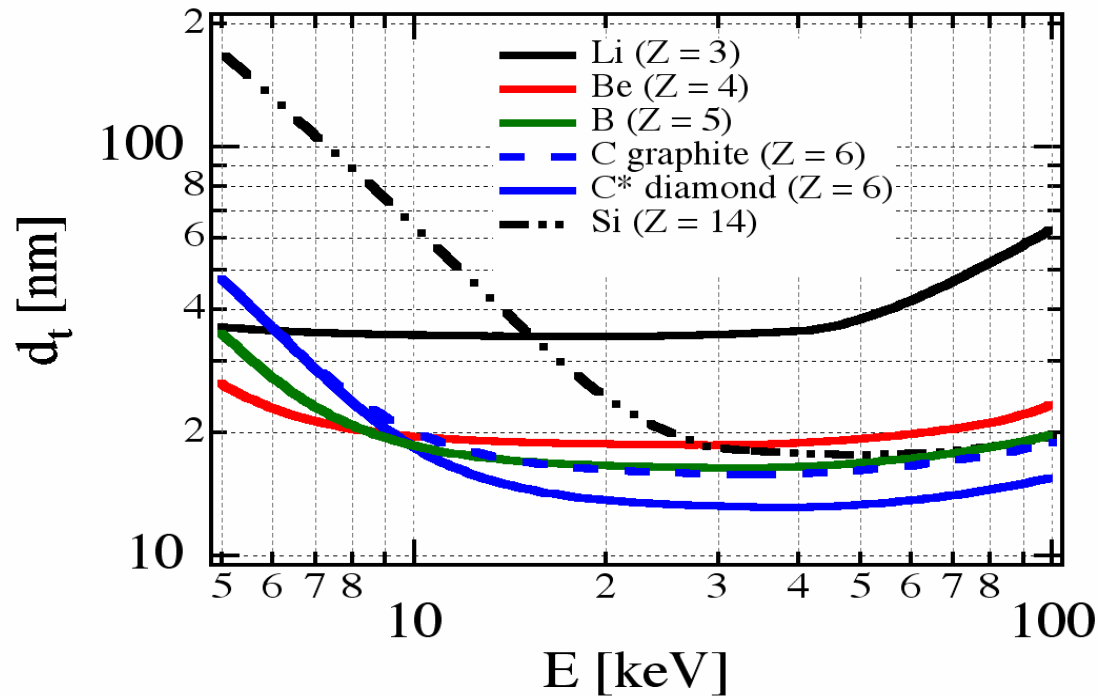
Limits diffraction limit of NFLs to

$$d_t \geq 0.75 \cdot \frac{\lambda}{2\sqrt{2\delta}} > 10\text{nm}$$

for useful lens materials

Effective Aperture and Diffraction Limit

Diffraction limit:



$$N = 100$$

$$l \geq 0.084$$

$$R = 0.5 - 50 \mu\text{m}$$

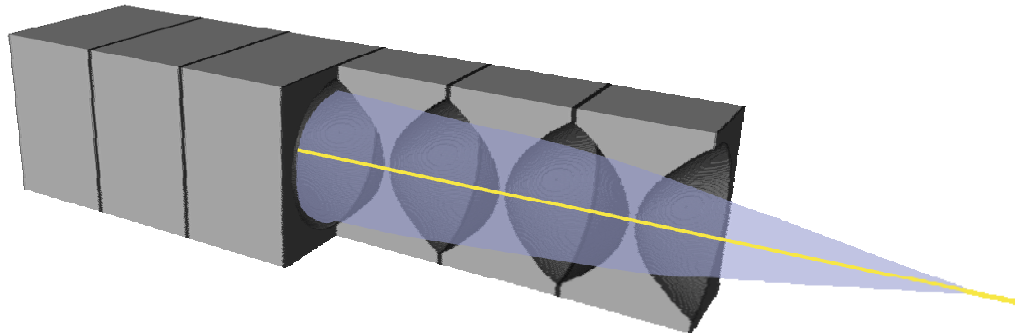
bounded by

$$0.75 \frac{\lambda}{2\sqrt{2\delta}} \propto \text{const.}$$

Best materials: high density and low Z

APL 82, 1485 (2003)

Refractive Power per Unit Length

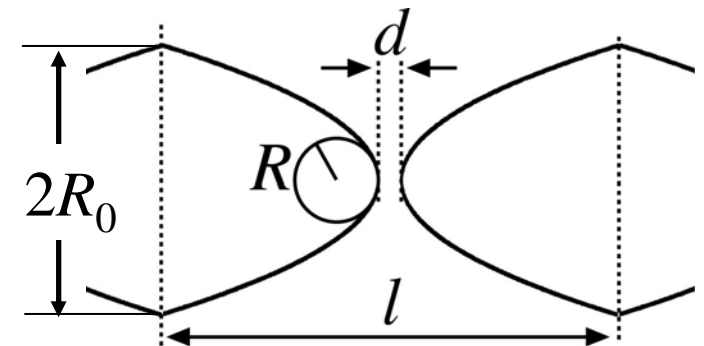


$$\omega^2 = \frac{1}{lf_s} = \frac{2\delta}{lR} \approx \frac{2\delta}{R_0^2}$$

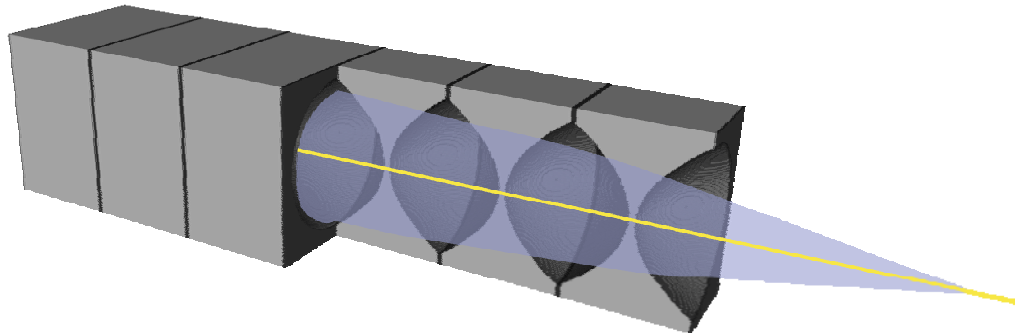
For large number of lenses:

$$r'' = \frac{d^2 r}{dz^2} = -\omega^2 r$$

Beam oscillates inside of lens
(analogy to harm. oscillator)



Refractive Power per Unit Length

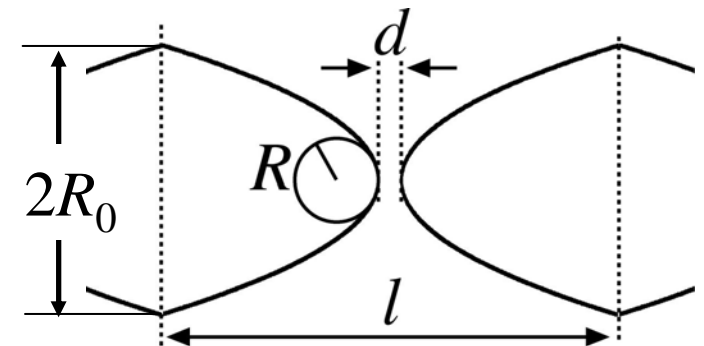


$$\omega^2 = \frac{1}{lf_s} = \frac{2\delta}{lR} \approx \frac{2\delta}{R_0^2}$$

- increases with decreasing R_0
- beam converges to focus inside of lens

aperture can be decreased
without loss toward exit of lens

increase ω^2 toward exit of lens



Adiabatically Focusing Lens

adjust R_0 to fit the converging beam as it is focused:

$$\omega^2 = \frac{2\delta}{l_j R_j} \approx \frac{2\delta}{R_{0j}^2}$$

Solve

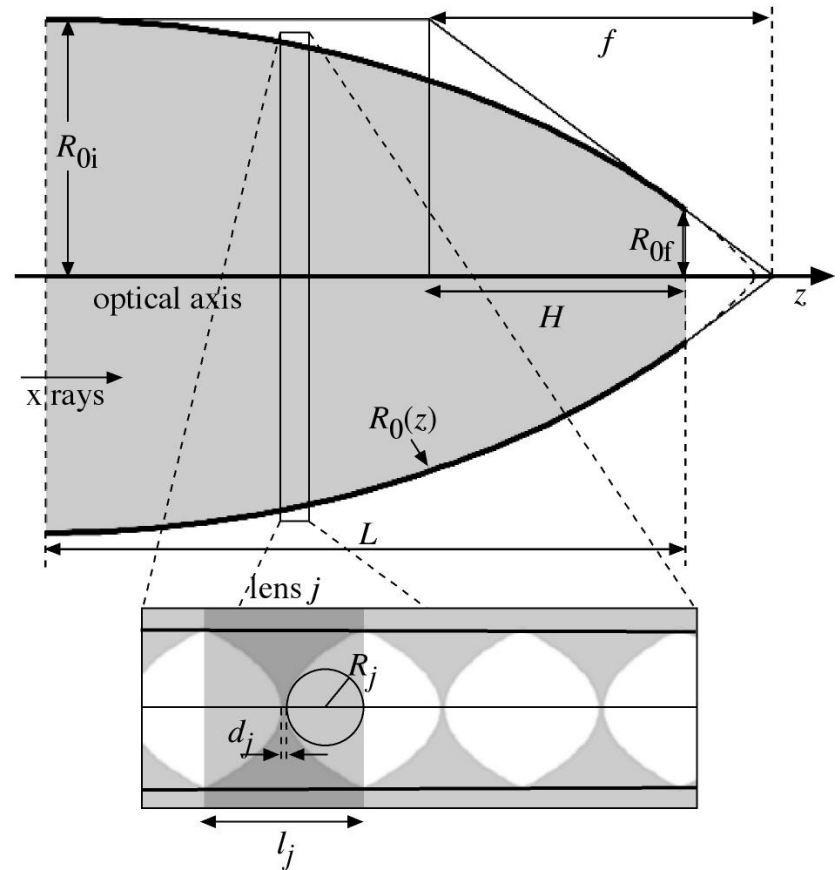
$$r'' = -\omega(z)r$$

for peripheral ray $R_0(z)$

PRL 94, 054802 (2005)

Cornell, 24.06.2006

adiabatically focusing lens (AFL)



Adiabatically Focusing Lens

$$R_0'' = -\frac{2\delta}{R_0}$$

First integral:

$$\frac{1}{2}(R_0')^2 + 2\delta \log(R_0) = E$$

E defined by initial conditions

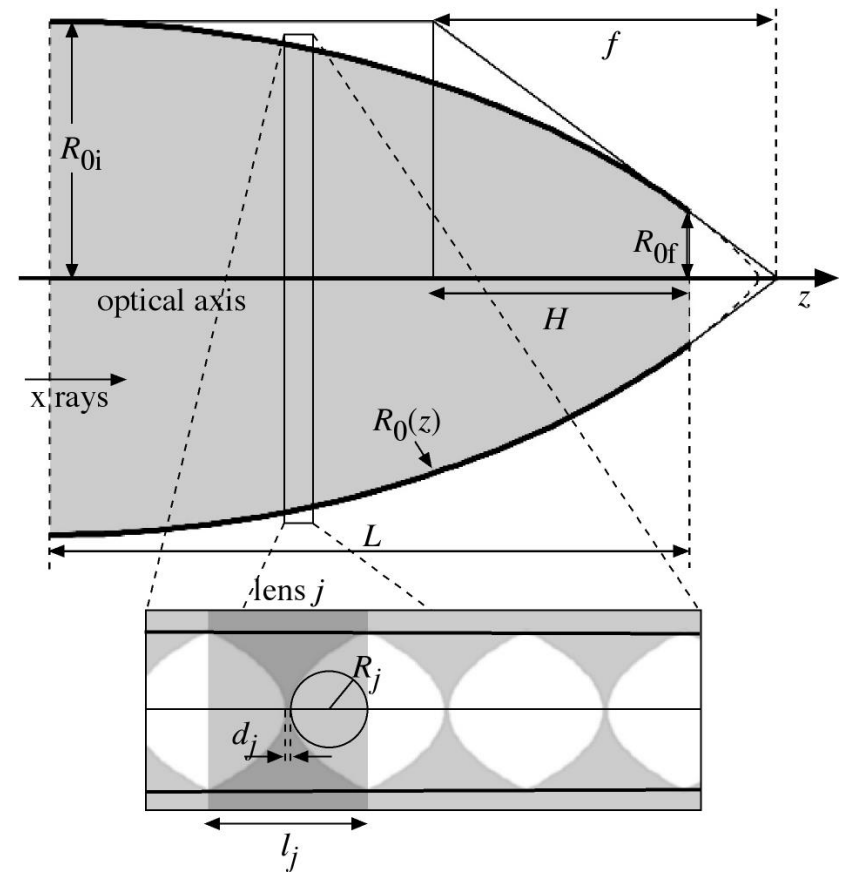
For example:

$$R_0' = 0, R_0 = R_{0i}$$

PRL 94, 054802 (2005)

Cornell, 24.06.2006

adiabatically focusing lens (AFL)



Adiabatically Focusing Lens

First order differential eq.:

$$R_0' = \sqrt{4\delta \log \frac{R_{0i}}{R_0}}$$

Solution shown to the right

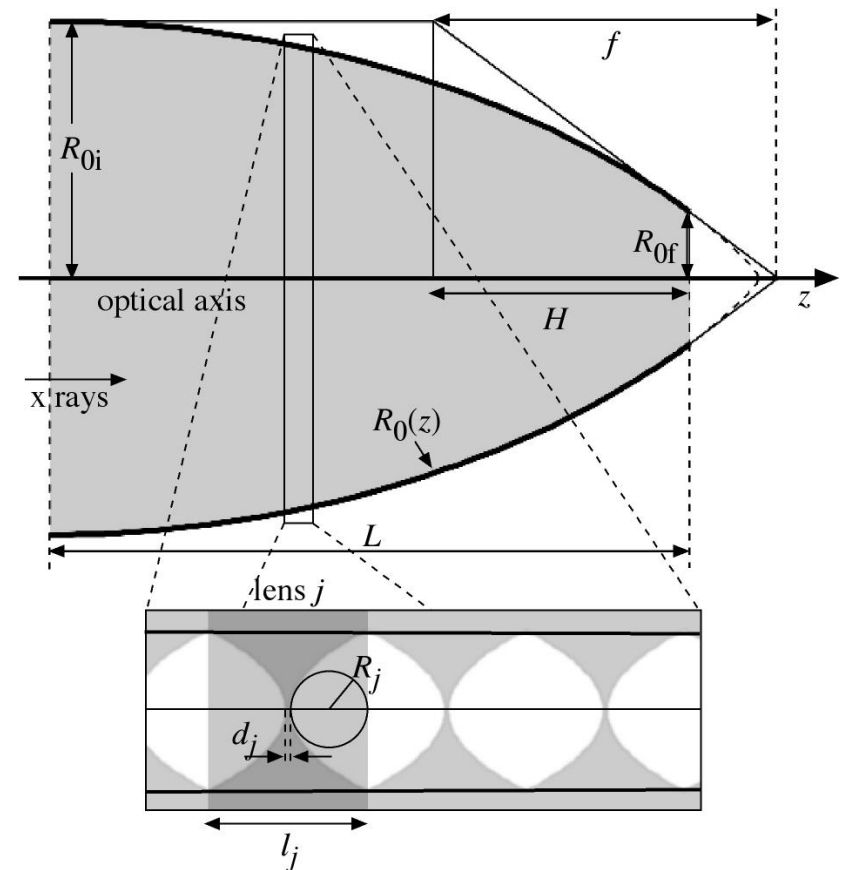
$$f = \frac{R_{0i}}{\sqrt{4\delta \log \frac{R_{0i}}{R_{0f}}}}$$

$$D_{\text{eff}} = 2R_{0i} \sqrt{\frac{2}{\mu L} \left[1 - \exp\left(-\frac{\mu L}{2}\right) \right]}$$

PRL 94, 054802 (2005)

Cornell, 24.06.2006

adiabatically focusing lens (AFL)



Adiabatically Focusing Lens

Numerical aperture:

(char. aperture)

$$NA = \sqrt{\delta} \sqrt{4 \frac{a}{R_{0i}} \left[1 - \exp\left(-\frac{R_{0i}}{a}\right) \right] \log \frac{R_{0i}}{R_{0f}}}, \text{ with } a = \frac{2\sqrt{\delta}}{\sqrt{\pi\mu}}$$

δ large: high density ρ } material parameters
 a large: low absorption (low Z) }

→ optimal material: diamond (high density, low Z)

R_{0i} set to maximize NA ($0.6 - 1 \cdot a$) } fabrication parameters
 R_{0f} set to minimal value }

PRL 94, 054802 (2005)

Cornell, 24.06.2006

Example AFL

Diamond lens:

low atomic number Z and high density ρ

$N = 1166$ individual lenses

entrance aperture: $18.9\mu\text{m}$

exit aperture: 100nm

$f = 2.3\text{mm}$

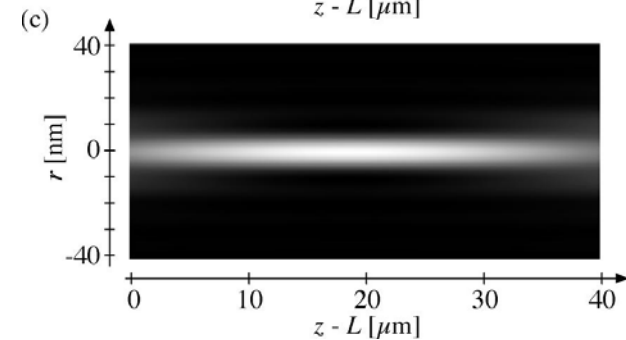
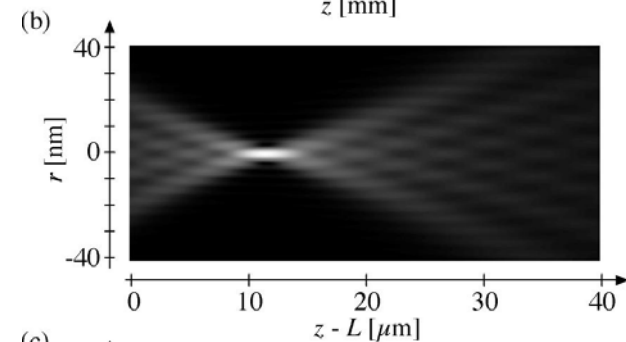
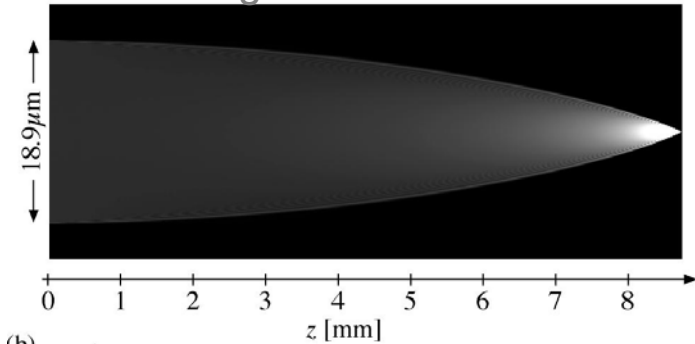
diffraction limit: 4.7nm

compare to NFL:

same aperture

diffraction limit: 14.2nm

(a) contracting wave field inside lens



Example AFL

Diamond lens:

low atomic number Z and high density ρ

$N = 1166$ individual lenses
 entrance aperture: $18.9\mu\text{m}$
 exit aperture: 100nm
 $f = 2.3\text{mm}$

diffraction limit: 4.7nm



Flux in focus (@20 keV, same focus size)

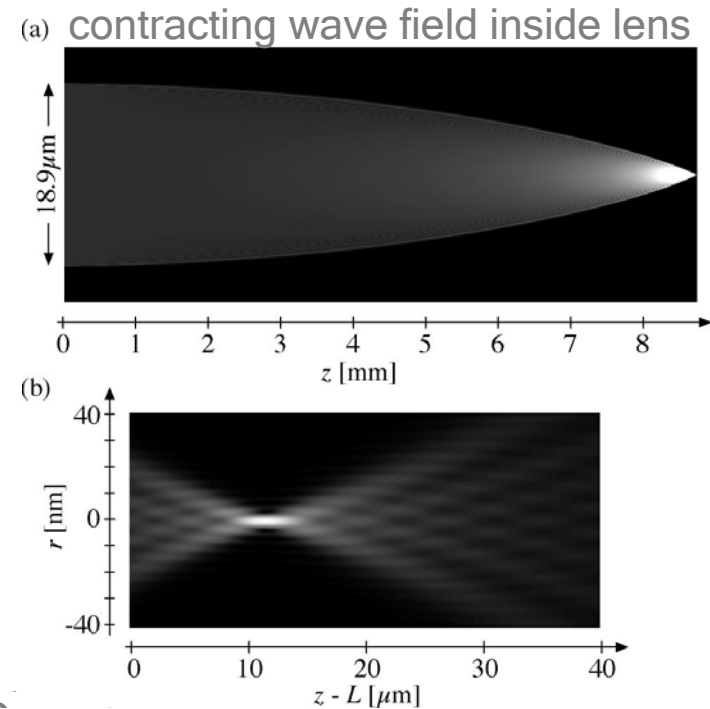
ERL hi-coh (15pm, 10mA): $\sim 10^{11}$ ph/s

ERL hi-coh (8pm, 25mA): $\sim 10^{12}$ ph/s

ESRF, Invac. undulator: $\sim 10^9$ ph/s

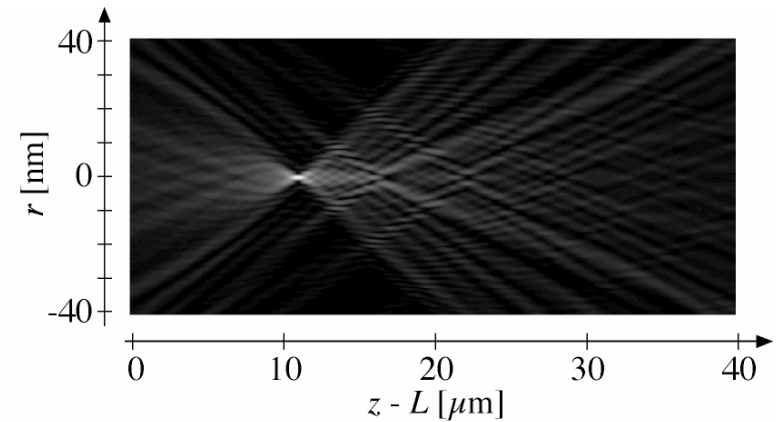
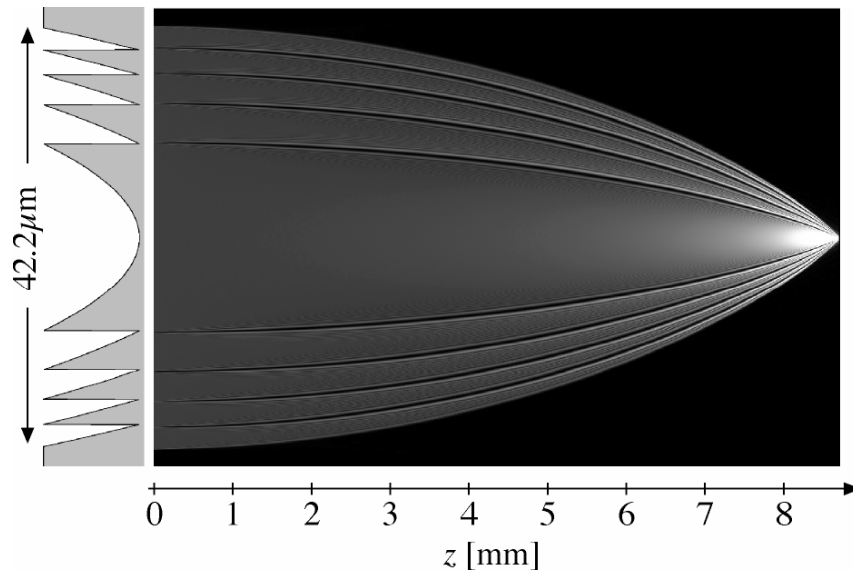
DOF = $1.1\mu\text{m}$

$\rightarrow 10^7 - 10^8$ ph/ $\text{\AA}^2/\text{s}$!!



Example AFL

kinoform lens: segment size follows converging beam



diffraction limit: 2.2nm

→ No sharp fundamental limit! Practical implementation difficult!

but

→ No atomic resolution in direct imaging with refractive lenses!

Refractive Lenses: Summary

Numerical aperture limited:

- limited density of low Z materials limits δ
- characteristic aperture a limits initial aperture R_{0i}
(as result of attenuation)
- fabrication and atomic structure limits exit aperture R_{0f}

Wave Propagation Through FZP

parabolic wave equation:

$$2ik \frac{\partial u}{\partial z} + \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + k^2 (n^2(x, y, z) - 1)u = 0$$

$n(x, y, z) = 1 - \delta(x, y, z) + i\beta(x, y, z)$ complex potential!

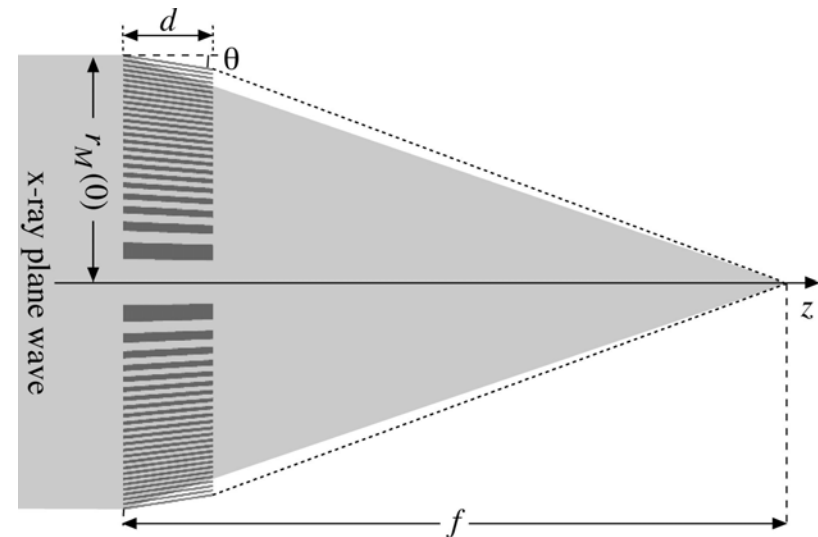
Ni/vac. zone plate

$E = 20 \text{ keV}$, $r_M(0) = 0.8 \mu\text{m}$

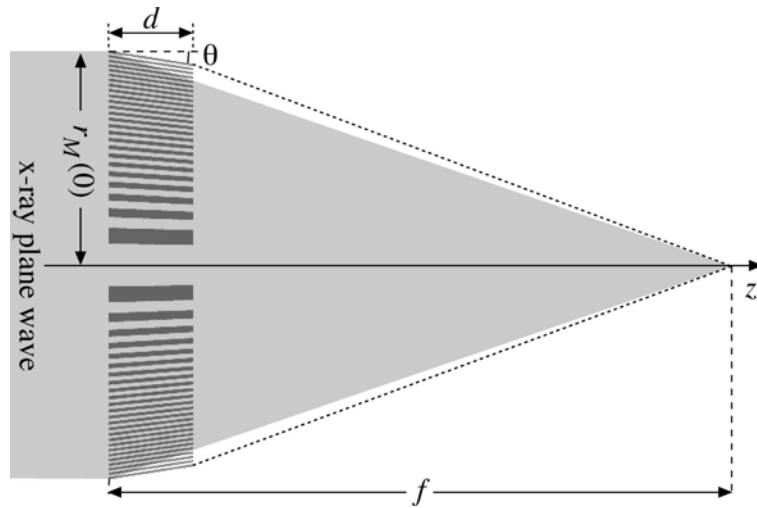
$\Delta r_M = 1 \text{ nm}$

(inspired by poster by
F. Pfeiffer at XRM2005)

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Wave Field Inside FZP

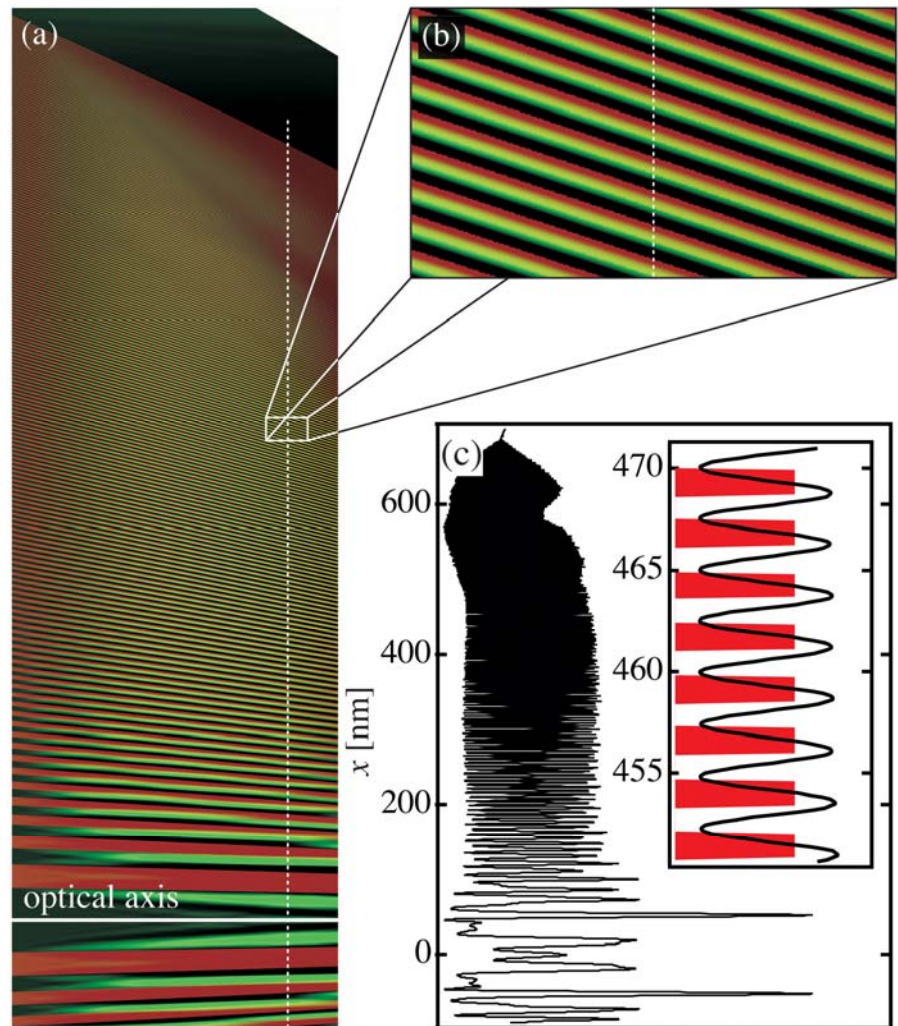


ideal tilted FZP

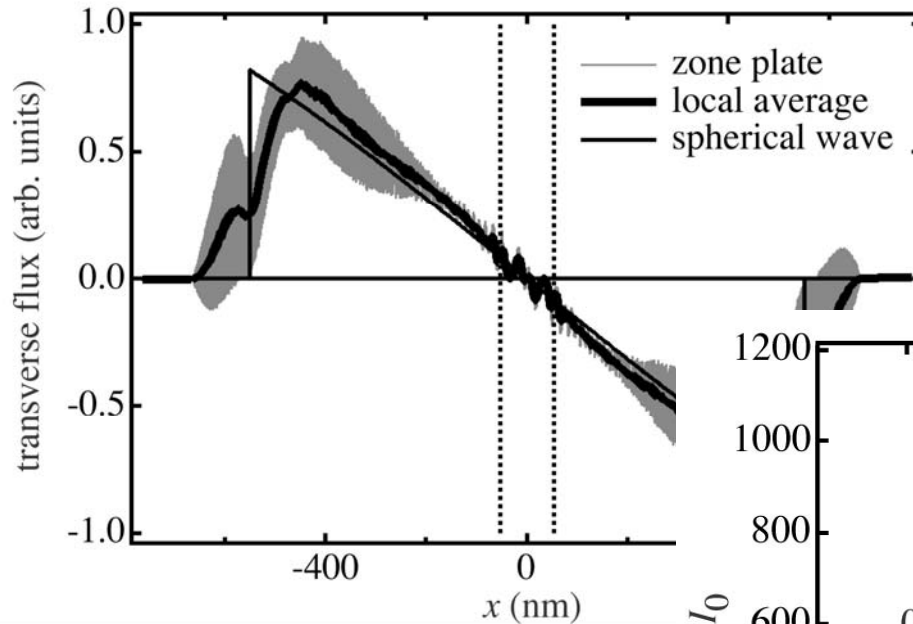
[Kang, et al., PRL 96 127401 (2006)]

incoming plane wave

propagate exit wave field
to focus

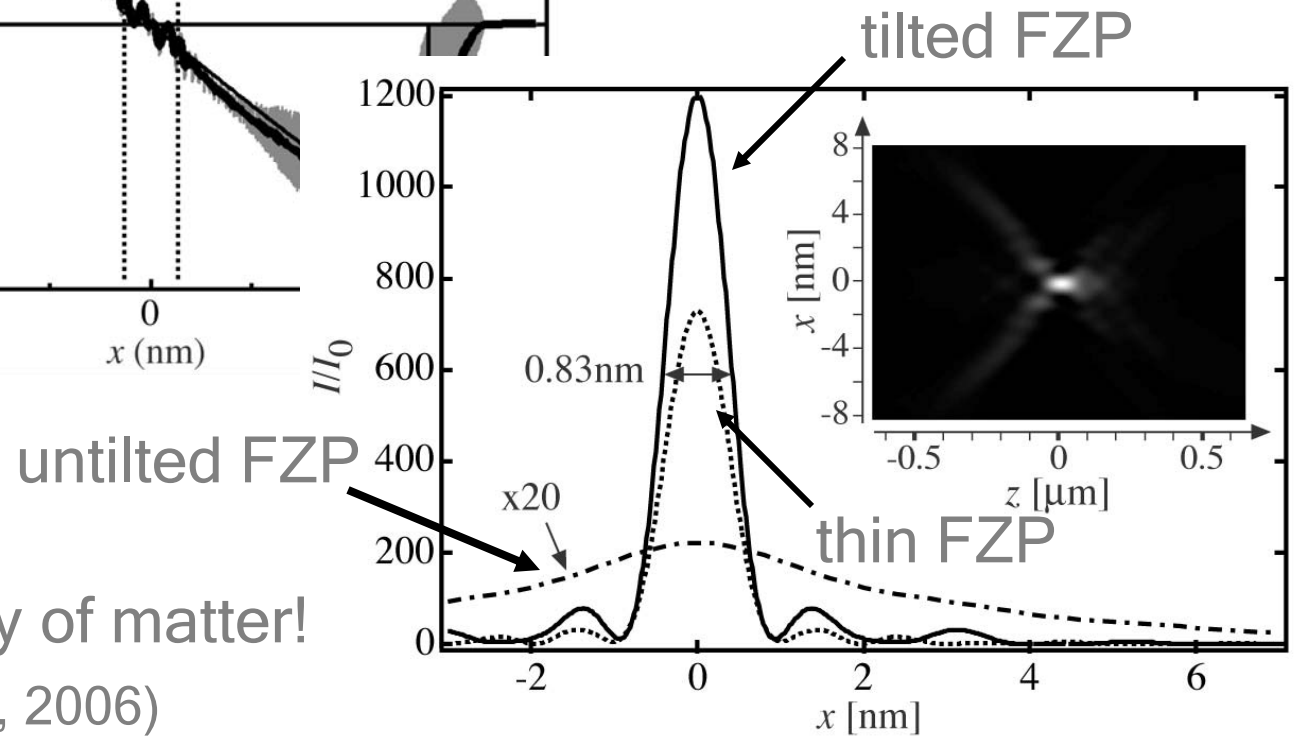


FZP Focus



transverse flux density:

$$J_x(x, z) = \frac{1}{2ik} [\langle \psi | \partial_x \psi \rangle - \langle \partial_x \psi | \psi \rangle]$$



Limit: atomicity of matter!

PRB, 74 (July 15, 2006)

Cornell, 24.06.2006

FZP: Summary

no limit as long as matter is homogeneous

multilayers have been shown to behave homogeneously
down to below 2 nm α -spacing (1 nm layers)

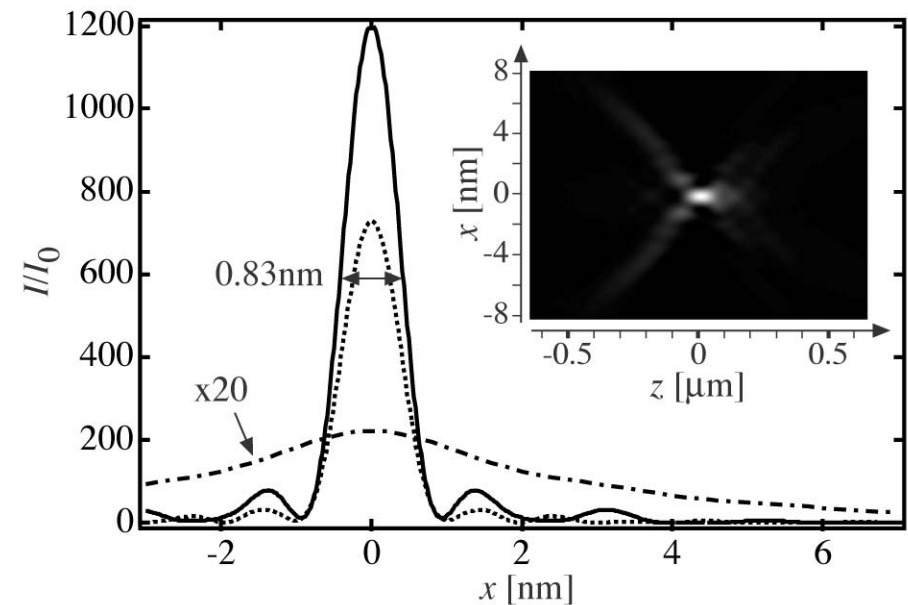
high efficiency, since only
one diffraction order is
excited!

atomicity will limit zone
placement!

other optics may be
calculated similarly!

PRB, 74 (July 15, 2006)

Cornell, 24.06.2006

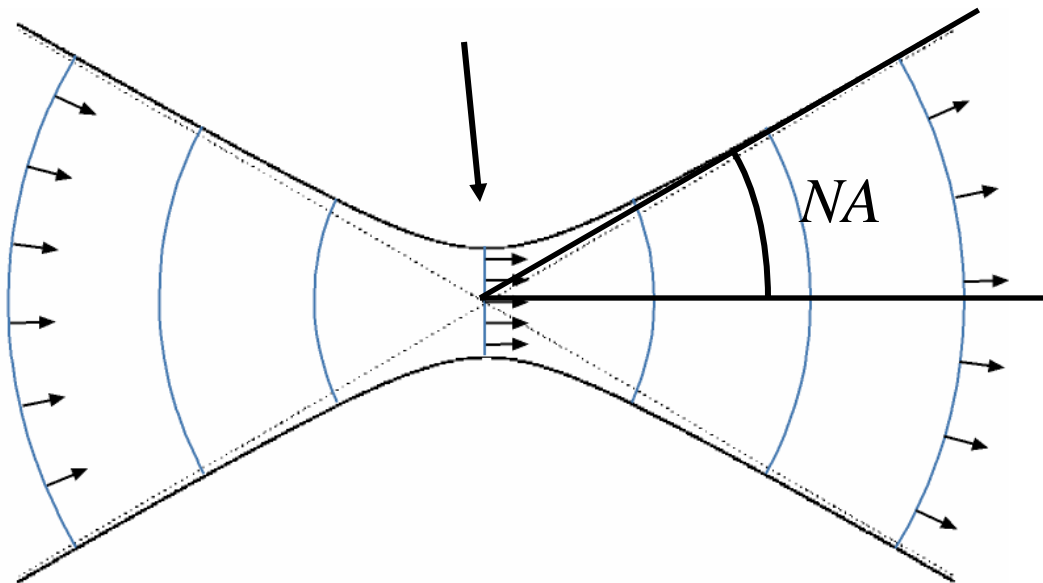


Wave Front in Diffraction Limited Focus

divergence angle:
numerical aperture

$$d_t = \frac{2\sqrt{2\ln 2}}{\pi} \frac{\lambda}{2NA} \approx 0.75 \frac{\lambda}{2NA}$$

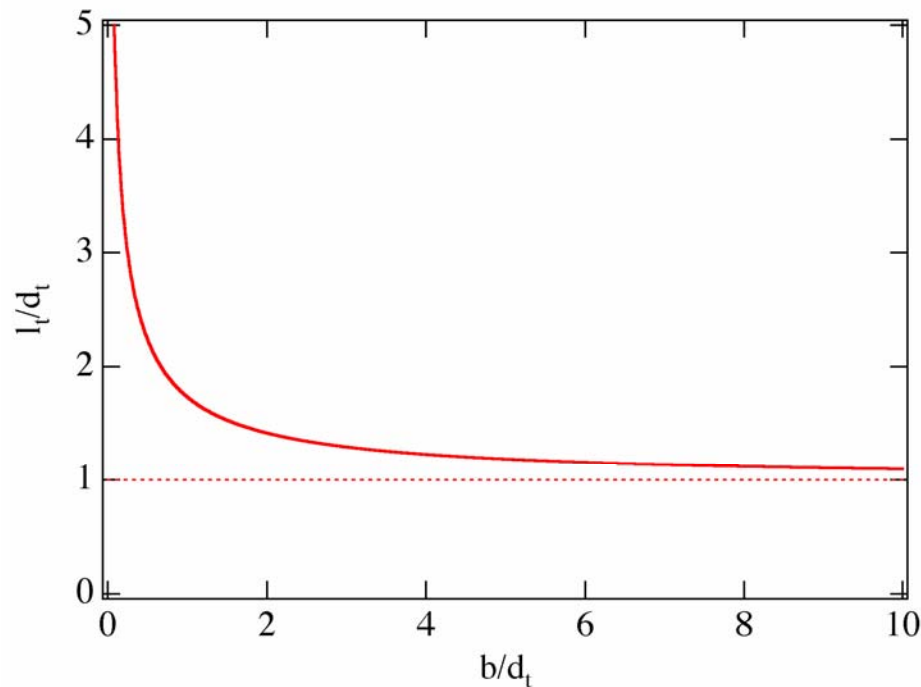
Gaussian limited plane wave



- coherent diffraction
- XPCS, XFCS

Wave Front in Diffraction Limited Focus

Lateral coherence length in nanofocused beam:



$$l_t = d_t \sqrt{1 + \frac{2d_t^2}{b^2}}$$

d_t : diffraction limit
 b : geometric image of source

Coherent diffraction at nanoparticles possible,
as long as particles are smaller than diffraction limit.

Coherence in the Focus

Si NFL @ ID13, $E = 15\text{keV}$
nominal parameters:

FWHM focus size:

66 x 75 nm²

diff. limit:

54 x 71 nm²



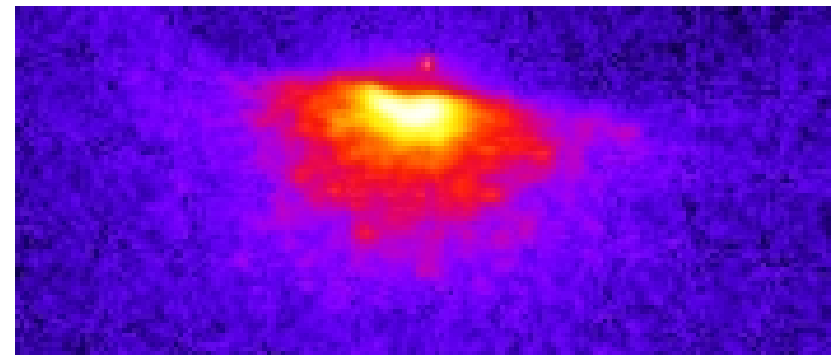
lateral coherence length:

120 x 300 nm²

divergence (NA):

0.58 x 0.43 mrad²

Preliminary experiment:
Diffraction from Fe-particles
($\sim 40\text{nm}$ diam., on Si_3N_4 membrane,
from R. Röhlberger)



(exposure: 10 s)

Visibility reduced:

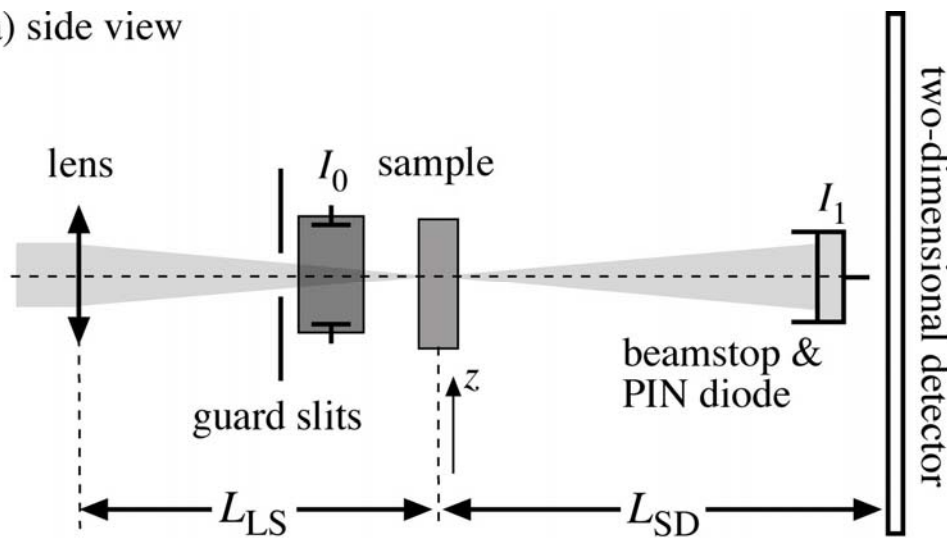
mechanical instability!

horiz. beam size: 120nm

Scanning Coherent Diffraction Microscopy

bridge the „small“ gap to atomic resolution by using coherent diffraction imaging contrast

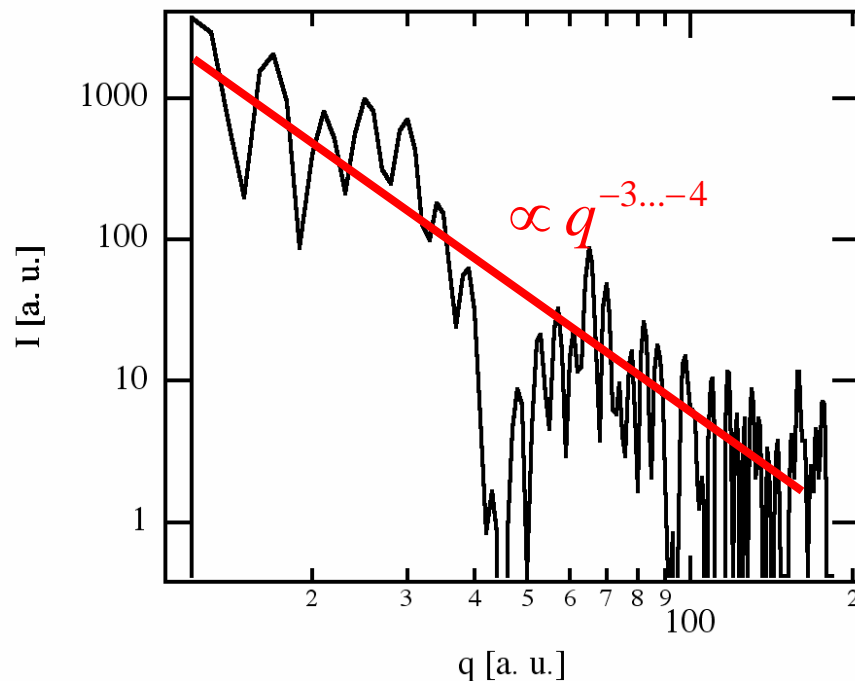
(a) side view



„arbitrary“ samples:
support defined
by illumination

Scanning Coherent Diffraction Microscopy

bridge the „small“ gap to atomic resolution by using coherent diffraction imaging contrast



smaller q -range (WAXS)

reduced requirements
on dynamic range of
detector

larger detector pixels

short local exposure
(up to $10^7 \text{ph}/\text{\AA}^2$)

Conclusion

Refractive optics:

- hard x-ray beams of 5nm seem feasible
(limiting factor is attenuation and atomicity of matter)
- kinoform lenses would reduce focus size (feasibility?)

Fresnel zone plates (tilted):

- focus below 1 nm should be feasible
(limiting factor is atomicity of matter)

Challenging experiment:

- scanning coherent diffraction microscopy

AFLs Made of Silicon

entrance aperture: $2R_{0i} = 20\mu\text{m}$
 exit aperture: $2R_{0f} = 1\mu\text{m}$
 energy: 10 - 20keV in 500eV steps

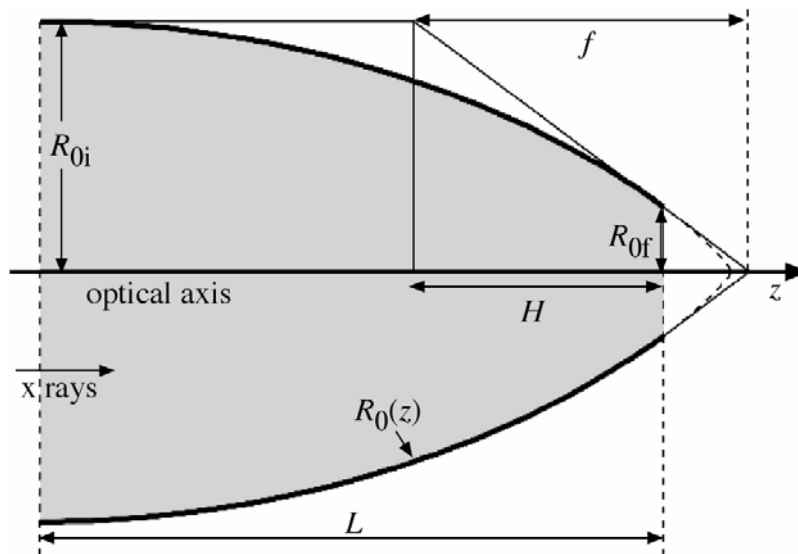
properties:

$$f = 2.7\text{mm}$$

$$d_t = 12.6\text{nm}$$

as horizontal lens in x-ray
nanoprobe (e. g. ID13 ESRF):

$$L_1 = 47\text{m}, \text{ source size: } 150\mu\text{m}$$

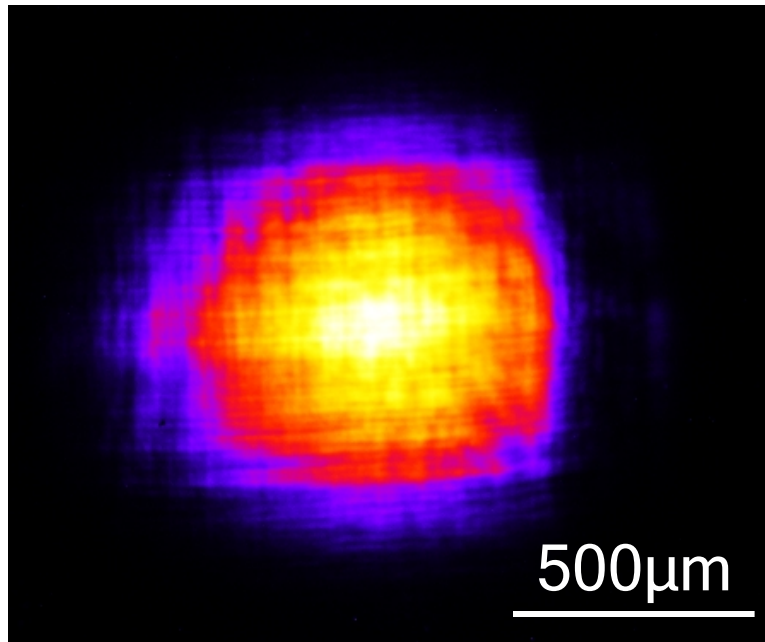


horizontal focus: 15.3nm
 (17400 x reduction)

Far Field of Focus: Aberrations

Si NFL @ ID13, $E = 15\text{keV}$

Far field image of focus:



detector dist.: 800mm

log (I)

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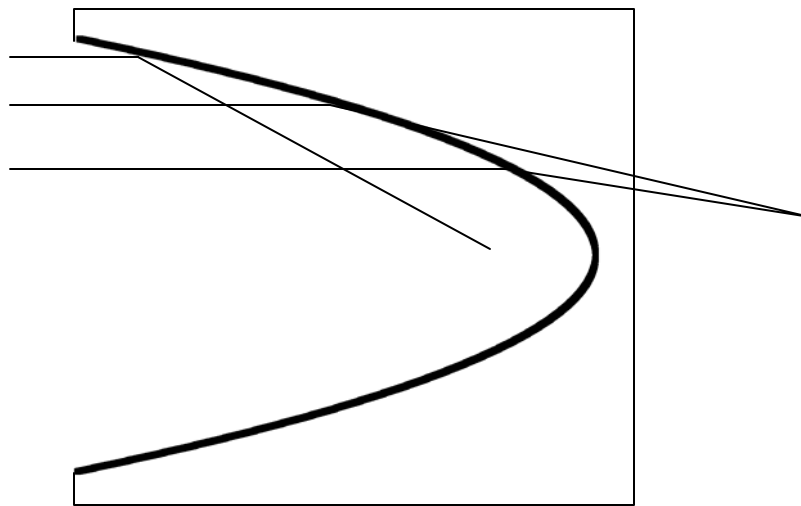
Structure:

irregularities in lens
shape

reconstruction of lens shape?
[Quiney, et al., Nat. Phys. 2, 101 (2006)]

Optimal Numerical Aperture of Single Lens

First scenario:



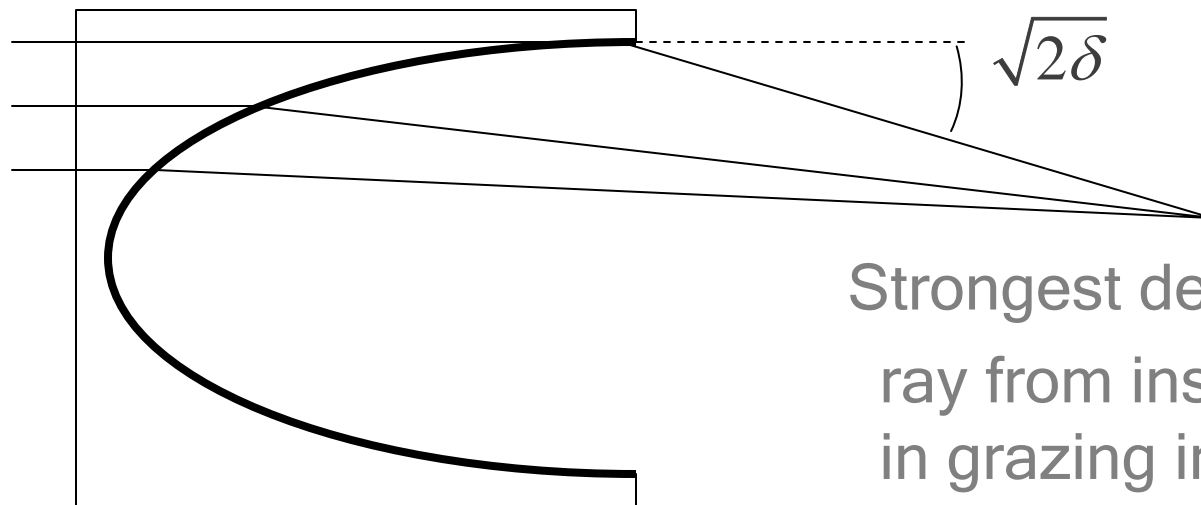
Works as long as ray is not totally reflected

Deflection angle $< \sqrt{2\delta}$

NA limited by $\sqrt{2\delta}$
even for non-absorbing material

Optimal Numerical Aperture of Single Lens

Second scenario:



Strongest deflection:

ray from inside the material
in grazing incidence

deflection angle $< \sqrt{2\delta}$

NA limited by $\sqrt{2\delta}$

→ make more than one refraction to increase NA