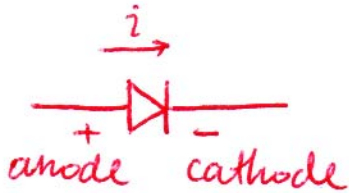


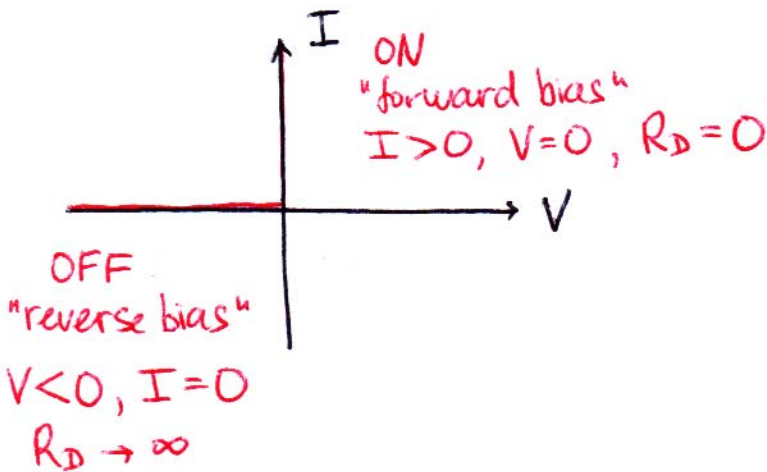
Lecture 13

Diodes

- 2 terminal passive nonlinear resistive device

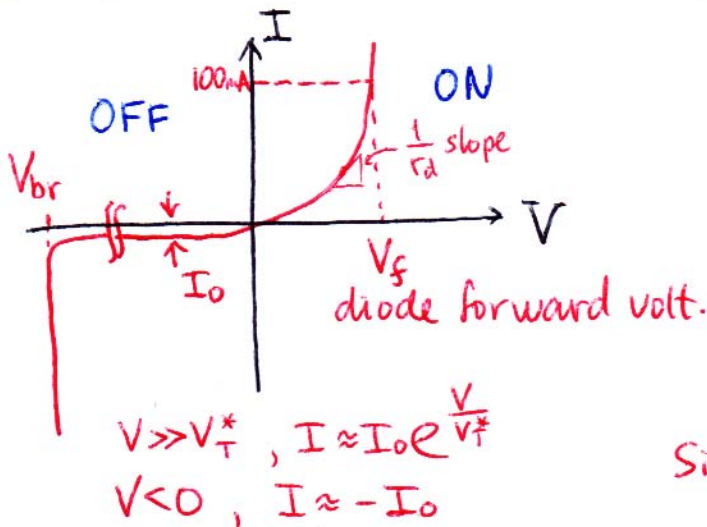


1) ideal diode



- like a switch (one way wire)
- curr. direction as shown in the symbol

2) real diode (semiconductor fab.)



Shockley equation

$$I = I_0 (e^{\frac{V}{V_T^*}} - 1)$$

- $I_0$  - "reverse satur. current"
- $V_T^*$  - "corrected therm. voltage"

Si diode:  $I_0 \sim 1 \text{ nA}, V_T^* \sim 40 \text{ mV}$

### 3) diode resistance

(2)

$$R_D = \frac{V}{I} = \frac{V}{I_0(e^{V/V_T^*} - 1)} = f(V) \quad \text{- nonlinear}$$

Differential (or slope) resistance

$$r_d = \frac{dV}{dI} = \frac{V_T^*}{I_0 e^{V/V_T^*}} \approx \frac{V_T^*}{I} \quad \text{for } V \gg V_T^*$$

### 4) modes of operation

Let  $V_T^* \sim 40 \text{ mV}$ ,  $I_0 \sim 1 \text{ nA}$

V	I (mA)	$R_D (\Omega)$	$r_d (\Omega)$	
0.1	$1.1 \times 10^{-5}$	$8.9 \times 10^6$	$3.3 \times 10^6$	} reverse bias (OFF)
0.2	$1.5 \times 10^{-4}$	$1.4 \times 10^6$	$2.7 \times 10^5$	
0.3	$1.8 \times 10^{-3}$	$1.7 \times 10^5$	$2.2 \times 10^4$	
0.4	$2.2 \times 10^{-2}$	$1.8 \times 10^4$	$1.8 \times 10^3$	
0.5	0.27	$1.9 \times 10^3$	150	} typical range of current $V \sim V_f \approx 0.6 \text{ V}$
0.6	3.3	180	12	
0.7	40	18	1.0	
0.8	490	1.7	0.08	
0.9	5900	0.15	0.007	
1.0	72000	0.01	0.0006	

#### Forward bias

typical I's  $\sim \text{mA to A}$

R's  $\sim 10 \Omega$  to  $\text{k}\Omega$

$V \sim V_f$  - "forward bias voltage"

$V_f \sim 0.6 \text{ V}$  Si

( $0.3 \text{ V}$  Ge  
 $1.5 \text{ V}$  GaAs) due to different  $I_0$

#### Reverse bias

OFF when  $V < V_f$  until  $V_{br}$

# 5) max ratings

③

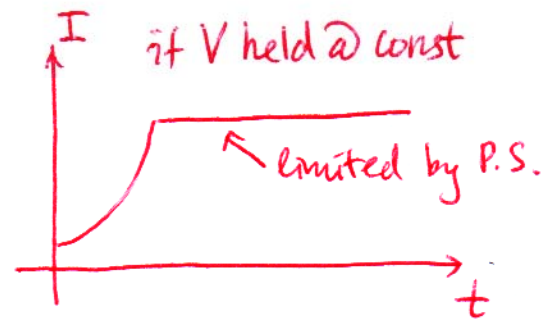
	signal 1N914	rectifier 1N4007
forward $I_{max}$ (DC)	$\sim 200\text{mA}$	1A
$V_{br}$	$\sim 100\text{V}$	$\sim 1000\text{V}$

Power dissipation on a diode  $P = I \cdot V$  (e.g. Si @  $0.8\text{V}$ ,  $P \approx 0.4\text{W}$ )

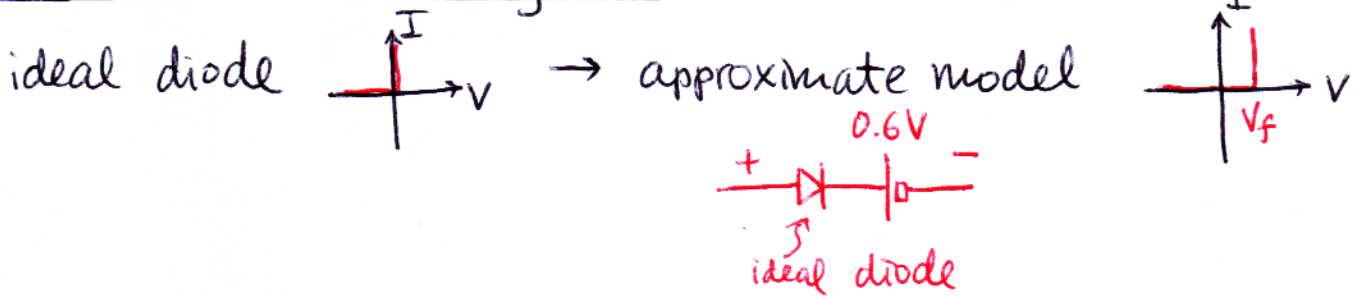
For fixed  $I$ ,  $\frac{dV}{dT} \approx -2\text{mV}/^\circ\text{C}$

E.g. fixed voltage bias:

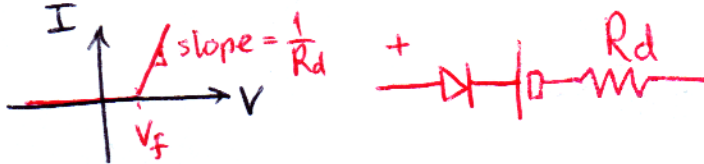
$\rightarrow T \uparrow, V \text{ cannot } \downarrow, \text{ so } I \uparrow \text{ and } P \uparrow$   
 $\Rightarrow$  thermal runaway possible



## Diode circuit analysis



$\rightarrow$  approximate resistive model



$\rightarrow$  Shockley eqn.

## Diode types

- signal: fast, small  $I$  (1N914)
- power (rectifier): large  $I$  (1N4007)

- Zener: <sup>in reverse breakdown</sup> const  $V_{br} = V_z$
- LED: GaAs, InP  $V_f \sim 1.5\text{-}2\text{V}$

# Diode applications

## ① rectifiers (turn AC → DC)

DC vs. AC - read "war of currents" on wikipedia

{	Thomas Edison = DC
	Nikolas Tesla = AC
	George Westinghouse = \$ for AC

High voltage lines: Q: why?

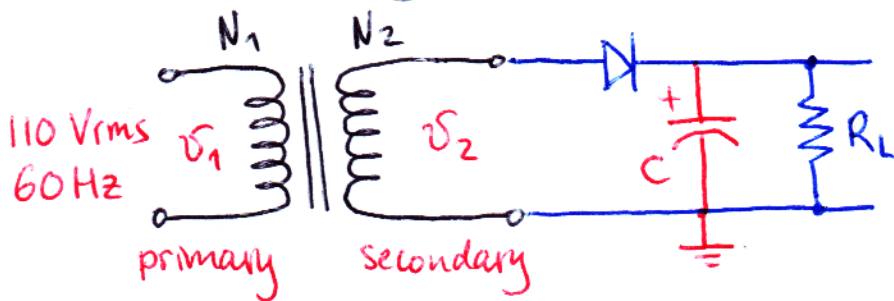
$P_{losses} = I^2 R_{losses}$  ;  $P = I \cdot V$  to be transmitted  $\Rightarrow$   
 $\uparrow$   
 useful curr.

$P_{losses} = \frac{P^2}{V^2} R_{losses}$   
 $\leftarrow$  use high volt.

To step down high volt:

only AC is economic soln.

DC power supply - converts AC to desired DC volt. level

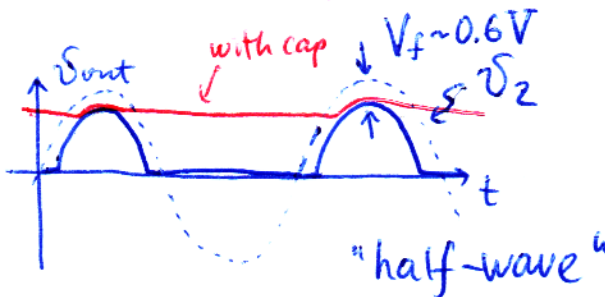


### i) transformer

$$\frac{V_2}{V_1} = \frac{N_2}{N_1}$$

- step AC voltage (up or down)

### ii) rectifier diode



### iii) filter cap

- add a cap such that  $\frac{1}{2\pi R_L C} \ll 60\text{Hz}$  (large  $R_L C$ )

$$\frac{dV}{dt} = \frac{I}{C}, \quad \frac{\Delta V_{out}}{T} = \frac{I_{load}}{C}, \quad \Rightarrow \Delta V_{out} = \frac{I_{load}}{C} \frac{1}{f} \leftarrow 60\text{Hz}$$