



# Lecture 6

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## 3. Linear transverse beam optics

### 3.1 Equation of motion

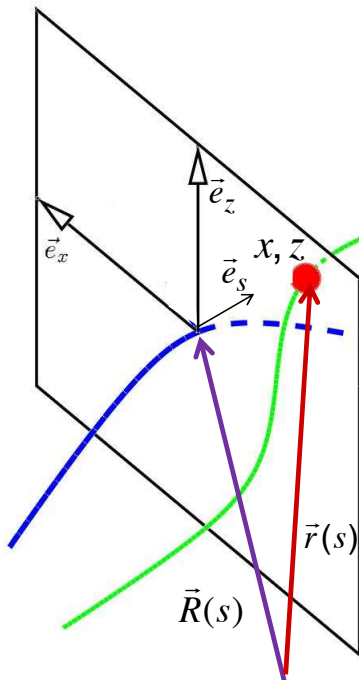
### 3.2 General solution of the equation of motion



## 3.1 Equation of motion in linear approximation



# A moving (curvi-linear) coordinate system



- use right handed coordinate system  $(x, z, s)$  that follows an ideal particle along the ideal path  
 ideal path = design orbit  
 has straight sections + curved sections with constant curvature  
 $\frac{1}{\rho} = \frac{q}{P}$   $\rho$  dipole  
 straight section:  $\rho = \infty \Leftrightarrow 1/\rho = 0$
- particle position vector:  
 $\vec{r} = \vec{R}(s) + x \vec{e}_x(s) + z \vec{e}_z(s)$   
 arc length along the design orbit  
 note:  $|\mathrm{d}\vec{R}| = \mathrm{d}s$      $\vec{e}_s = \frac{\mathrm{d}}{\mathrm{d}s} \vec{R}(s)$



# Equation of Motion (I)

$$\frac{\mathrm{d}^2 \vec{r}}{\mathrm{d}t^2} = \vec{f}_r(\vec{r}, \frac{\mathrm{d}}{\mathrm{d}t} \vec{r}, t)$$

3 dimensional ODE of 2<sup>nd</sup> order can be changed to a  
 6 dimensional ODE of 1<sup>st</sup> order:

$$\left. \begin{aligned} \frac{\mathrm{d}}{\mathrm{d}t} \vec{r} &= \frac{1}{m\gamma} \vec{p} = \frac{c}{\sqrt{p^2 - (mc)^2}} \vec{p} \\ \frac{\mathrm{d}}{\mathrm{d}t} \vec{p} &= \vec{F}(\vec{r}, \vec{p}, t) \end{aligned} \right\} \frac{\mathrm{d}}{\mathrm{d}t} \vec{Z} = \vec{f}_Z(\vec{Z}, t), \quad \vec{Z} = (\vec{r}, \vec{p})$$

If the force does not depend on time, as in a typical beam line magnet, the energy is conserved so that one can reduce the dimension to 5.

Furthermore, the time dependence is often not as interesting as the trajectory along the accelerator length "s". Using "s" as the independent variable reduces the dimensions to 4.

$$\frac{\mathrm{d}}{\mathrm{d}s} \vec{z} = \vec{f}_z(\vec{z}, s), \quad \vec{z} = (x, y, p_x, p_y)$$



## Equation of Motion (II)

Usually one prefers to compute the trajectory as a function of “s” along the accelerator even when the energy is not conserved, as when accelerating cavities are in the accelerator.

Then the energy “E” and the time “t” at which a particle arrives at the cavities are important. And the equations become **6 dimensional** again:

$$\frac{d}{ds} \vec{z} = \vec{f}_z(\vec{z}, s), \quad \vec{z} = (x, y, p_x, p_y, -t, E)$$



## Equation of motion in linear approximation

In the following:

– look at transverse motion only:

$$x, z, \quad x' = \frac{dx}{ds} = \frac{dx}{dt} \frac{dt}{ds} = \frac{v_x}{v_s} = \frac{p_x}{p_s} \approx \frac{p_x}{p_0}$$

$$z' = \frac{dz}{ds} = \frac{dz}{dt} \frac{dt}{ds} = \frac{v_z}{v_s} = \frac{p_z}{p_s} \approx \frac{p_z}{p_0}$$

in addition: need  $\delta = \frac{E - E_0}{E_0} \approx \frac{p - p_0}{p_0} \leftarrow$  design momentum

– assume only linear, constant magnetic fields (transverse), no electric fields

dipole + quad. only!

$$\begin{cases} B_x = \pm \frac{p_0}{q} k z \\ B_z = \frac{p_0}{q} \frac{1}{S} + \frac{p_0}{q} k x \end{cases}$$

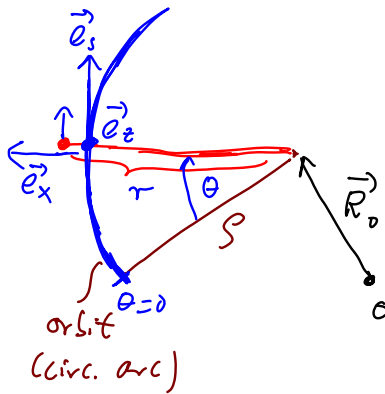
$\leftarrow$  quadrupole strength       $\leftarrow$   $1/S$  = curvature in dipole field

– only consider first order terms in small quantities

$\Rightarrow$  equ. of motion in linear approximation!   
  $\Rightarrow$  not too small bending radii!



## Equation of motion in linear approximation



particle position vector:

$$\vec{r} = \vec{R}_0 + \rho \vec{e}_x + z \vec{e}_z$$

$$\rho = \rho + x$$

for small  $d\theta$  (cylindrical coordinates!)

$$d\vec{e}_x \leftarrow \begin{matrix} \vec{e}_x(\theta+d\theta) \\ \vec{e}_x(\theta) \end{matrix} d\theta \quad d\vec{e}_x = d\theta \vec{e}_s$$

$$\begin{matrix} d\vec{e}_s \\ \vec{e}_s(\theta) \\ \vec{e}_s(\theta+d\theta) \end{matrix} d\theta \quad d\vec{e}_s = -d\theta \vec{e}_x$$

$$d\vec{e}_z = 0$$

$$\Rightarrow \frac{d\vec{r}}{dt} = \dot{\vec{r}} = \dot{\rho} \vec{e}_x + \rho \dot{\vec{e}}_x + \dot{z} \vec{e}_z = \dot{\rho} \vec{e}_x + \rho \dot{\theta} \vec{e}_s + \dot{z} \vec{e}_z$$

$\nearrow d\vec{e}_x/dt = d\theta/dt \vec{e}_s$



## Equation of motion in linear approximation

$\Rightarrow$  for acceleration:

$$\ddot{\vec{r}} = (\ddot{\rho} - \rho \dot{\theta}^2) \vec{e}_x + (2\dot{\rho}\dot{\theta} + \rho \ddot{\theta}) \vec{e}_s + \ddot{z} \vec{e}_z$$

$\leftarrow = 0$  here (no longitudinal acceleration)

• now:  $\vec{F} = \frac{d\vec{p}}{dt} = \gamma m \ddot{\vec{r}}$  since  $\gamma = \text{const}$  here ( $\vec{F} \perp \vec{v}$ )

$$\Rightarrow m \ddot{\vec{r}} = q \vec{v} \times \vec{B} = q [\dot{z} B_s - \rho \dot{\theta} B_z] \vec{e}_x + (\dot{\rho} B_z - \dot{z} B_x) \vec{e}_s + (\rho \dot{\theta} B_x - \dot{\rho} B_s) \vec{e}_z$$

$\Rightarrow$  assume  $B_s = 0$  tangential fields only

$$m (\ddot{\rho} - \rho \dot{\theta}^2) = -q \rho \dot{\theta} B_z(x, z, s)$$

$$m \dot{z} = q \rho \dot{\theta} B_x(x, z, s)$$

$\Rightarrow$  for linear beam optics:

$$B_x = \pm g z = \pm \frac{p_0}{q} k z$$

$$B_z = B_0 \pm g x = \frac{p_0}{q} \frac{1}{\rho} \pm k x$$



## Equation of motion in linear approximation

$\Rightarrow$  with  $r = \rho + x$ ,  $\rho = \text{const}$  within given dipole magnet

$$m(\ddot{x} - r\dot{\theta}^2) = -r\dot{\theta} \left( p_0 \frac{1}{\rho} \pm p_0 kx \right)$$

$$m\ddot{z} = \pm r\dot{\theta} p_0 k z$$

$\Rightarrow$  since  $v_s = r\dot{\theta} \gg v_x, v_z$

$$\Rightarrow v_s = r\dot{\theta} \approx |\vec{v}|$$

$\Rightarrow$  also: replace time variable by arc length  $s$  along design orbit:

$$s = vt \Rightarrow \ddot{x} = \frac{d^2x}{dt^2} = \frac{d^2x}{ds^2} \left( \frac{ds}{dt} \right)^2 = x'' v^2$$

$$\ddot{z} = z'' v^2$$

$$\Rightarrow x'' \pm \frac{p_0}{\rho} kx = \frac{1}{r} - \frac{p_0}{\rho} \frac{1}{\rho} \qquad z'' \mp \frac{p_0}{\rho} kz = 0$$



## Equation of motion in linear approximation

particle momentum:  $p = p_0 (1 + \delta)$   $\delta = \frac{\Delta p}{p_0}$  momentum error of particle

$\Rightarrow$  to first order approximation:

$$\text{for } \delta \ll 1: \frac{1}{p} = \frac{1}{p_0(1+\delta)} \approx \frac{1}{p_0} (1 - \delta)$$

$$\text{for } \rho \gg x: \frac{1}{r} = \frac{1}{\rho(1+x/\rho)} \approx \frac{1}{\rho} \left( 1 - \frac{x}{\rho} \right)$$

$\Rightarrow$  to first order in  $x, z, \delta$ :

$$x'' + \left( \pm k + \frac{1}{\rho^2} \right) x = \frac{\delta}{\rho} \left( + \mathcal{O}(2) + \mathcal{O}(3) + \dots \right)$$

$$z'' \mp kz = 0 \left( + \mathcal{O}(2) + \mathcal{O}(3) + \dots \right)$$

equ. of transverse motion in linear beam optics



## Equation of motion in linear approximation

- $1/\rho^2$  term: "weak focussing" in dipole magnet
  - in dipole:  $k=0$
  - in quadrupole:  $1/\rho=0$
  - in drift:  $k=0$ ,  $1/\rho=0$
- Note: all terms on the right-hand side can be treated as small perturbations!



## 3.2 General solution of the equation of motion



## linear, unperturbed equation of motion

have homogeneous differential equation:

$$(eq. 1) \quad u'' + \underbrace{\mathcal{K}(s)}_{\text{"}\omega^2\text{"}} u = 0 \quad \left. \vphantom{\mathcal{K}(s)} \right\} \begin{array}{l} \text{like harmonic oscillator} \\ \text{with time-dep. / s-dep.} \\ \text{frequency} \end{array}$$

where  $u$  stands for  $x$  or  $z$

$$\text{and } \mathcal{K} = \pm k + \frac{1}{s^2} \quad \text{or} \quad \mathcal{K} = \mp k \quad \text{for given magnet}$$

$\Rightarrow$  principal solutions (there should be two linearly indep. solutions!) for  $\mathcal{K} = \text{const.}$ :

$$\text{for } \mathcal{K} > 0 \quad C(s) = \cos(\sqrt{\mathcal{K}}s) \quad \text{and} \quad S(s) = \frac{1}{\sqrt{\mathcal{K}}} \sin(\sqrt{\mathcal{K}}s)$$

$$\text{for } \mathcal{K} < 0 \quad C(s) = \cosh(\sqrt{|\mathcal{K}|}s) \quad \text{and} \quad S(s) = \frac{1}{\sqrt{|\mathcal{K}|}} \sinh(\sqrt{|\mathcal{K}|}s)$$



with initial conditions:

$$C(0) = 1 \quad C'(0) = \left. \frac{dC}{ds} \right|_0 = 0$$

$$S(0) = 0 \quad S'(0) = \left. \frac{dS}{ds} \right|_0 = 1$$

(eq. 2)

$\Rightarrow$  any arbitrary solution  $u(s)$  can be expressed as a linear combination of these two principal solutions:

$$\left. \begin{array}{l} u(s) = C(s)u_0 + S(s)u_0' \\ u'(s) = C'(s)u_0 + S'(s)u_0' \end{array} \right\} \text{(eq. 3)}$$

where  $u_0$  and  $u_0'$  are the initial values of  $u(s)$  and  $u'(s)$  at  $s=0$



- general beam line with several magnets:

$$\mathcal{K} = \mathcal{K}(s)$$

$\Rightarrow$  principle solutions (so-called *sine like and cosine like solutions*) can be found with initial conditions as above for  $\mathcal{K} = \text{const}$  case!

$$\left[ u'' + \mathcal{K}(s) u = 0 \quad \text{insert ansatz (eqn 3)} \right]$$

$$\Rightarrow [s''(s) + \mathcal{K}(s) s(s)] u_0 + [c''(s) + \mathcal{K}(s) c(s)] u_0' = 0$$

for any initial condition  $(u_0, u_0')$

$$\Rightarrow s''(s) + \mathcal{K}(s) s(s) = 0$$

$$c''(s) + \mathcal{K}(s) c(s) = 0$$

i.e. general solution can be written as a sum of two linearly independent solutions  $(c(s) \text{ and } s(s))$



## Matrix formulation:

now: solution (eq. 3) of equ. of motion (1)  
in matrix formulation

$$\begin{bmatrix} u(s) \\ u'(s) \end{bmatrix} = \begin{bmatrix} c(s) & s(s) \\ c'(s) & s'(s) \end{bmatrix} \begin{bmatrix} u_0 \\ u_0' \end{bmatrix}$$

at exit  
of beamline/  
magnet

transformation  
matrix of given  
beamline/magnet

initial  
condition

$\Rightarrow$  from  $\mathcal{K} = \text{const}$  solutions: can obtain transformation matrix for each individual beam line element (magnet)

$\Rightarrow$  by repeated matrix multiplication, can follow particle trajectory along a complicated beam line!