



Lecture 9

3. Linear transverse beam optics

3.4 Transformation matrices of accelerator magnets

Quadrupole
 Combined function magnet
 Thin lens approximation

3.5 Momentum compaction Factor

3.6 Twiss parameters ($\alpha, \beta, \gamma, \psi$)



d) Quadrupole: of length l

d₁) horizontal defocusing, vertical focusing

$$\frac{1}{\rho} = 0, \quad \mathcal{K}_x = -k < 0 \quad \mathcal{K}_z = k > 0$$

$$\Rightarrow C_x = \cosh(\sqrt{k} l) \quad S_x = \frac{1}{\sqrt{k}} \sinh(\sqrt{k} l)$$

$$C_z = \cos(\sqrt{k} l) \quad S_z = \frac{1}{\sqrt{k}} \sin(\sqrt{k} l)$$

$$D_x = 0, \quad D_z = 0 \quad M_{56} = 0 \quad \vec{F} = \vec{0}$$

$$\Rightarrow M_{\text{quad}} = \begin{bmatrix} \cosh(\sqrt{k} l) & \frac{1}{\sqrt{k}} \sinh(\sqrt{k} l) & 0 & 0 \\ \sqrt{k} \sinh(\sqrt{k} l) & \cosh(\sqrt{k} l) & 0 & 0 \\ 0 & 0 & \cos(\sqrt{k} l) & \frac{1}{\sqrt{k}} \sin(\sqrt{k} l) \\ 0 & 0 & -\sqrt{k} \sin(\sqrt{k} l) & \cos(\sqrt{k} l) \end{bmatrix}$$



d₂) horizontal focusing, vertical defocusing

$$1/p = 0 \quad \mathcal{K}_x = k > 0 \quad \mathcal{K}_z = -k < 0$$

replace $C_x \leftrightarrow C_z$
 $S_x \leftrightarrow S_z$

$$M_{\text{quad}} = \begin{bmatrix} \cos(\sqrt{k}l) & \frac{1}{\sqrt{k}} \sin(\sqrt{k}l) & 0 & 0 \\ -\sqrt{k} \sin(\sqrt{k}l) & \cos(\sqrt{k}l) & 0 & 0 \\ 0 & 0 & \cosh \sqrt{k}l & \frac{1}{\sqrt{k}} \sinh \sqrt{k}l \\ 0 & 0 & \sqrt{k} \sinh \sqrt{k}l & \cosh \sqrt{k}l \end{bmatrix}$$

horiz. foc.



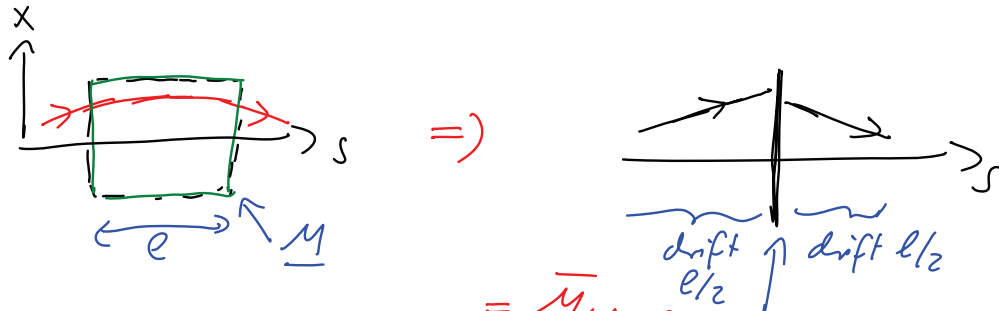
e) combined function bend:

$$\mathcal{K}_x = \pm k + \frac{1}{\rho^2} \quad \mathcal{K}_z = \mp k$$

=> see homework



f) thin lens approximation



$$\vec{X} = \underline{M} \vec{X}_0 = \underline{M}_{\text{drift } e/2} \underline{M}_{\text{drift } -e/2} \underline{M}_{\text{thin lens}} \underline{M}_{\text{drift } -e/2} \underline{M}_{\text{drift } e/2} \vec{X}_0$$

for thin drift:

$$\underline{M}_{\text{thin drift}} = \underline{M}_{\text{drift } -e/2} \underline{M}_{\text{drift } e} \underline{M}_{\text{drift } -e/2} = 1$$



f₁) thin, weak lens dipole: for $e/\rho \ll 1$

$$\underline{M}_{\text{thin bend}} = \underline{M}_{\text{drift } -e/2} \underline{M}_{\text{bend}} \underline{M}_{\text{drift } -e/2} \approx \begin{bmatrix} 1 & 0 & 0 & 0 \\ -e/\rho^2 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -e/\rho & 0 & 0 & 1 \end{bmatrix}$$

f₂) thin, weak lens quadrupole: $\sqrt{k} e \ll 1$, $ke = 1/\rho$

$$\underline{M}_{\text{thin quad vert foc.}} = \underline{M}_{\text{drift } -e/2} \underline{M}_{\text{quad vert foc.}} \underline{M}_{\text{drift } -e/2} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ ke & 1 & 0 & 0 \\ 0 & -ke & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



f₃) thin, weak combined function bend \rightarrow see HW

Note: in all cases (even for thin lens approximation)

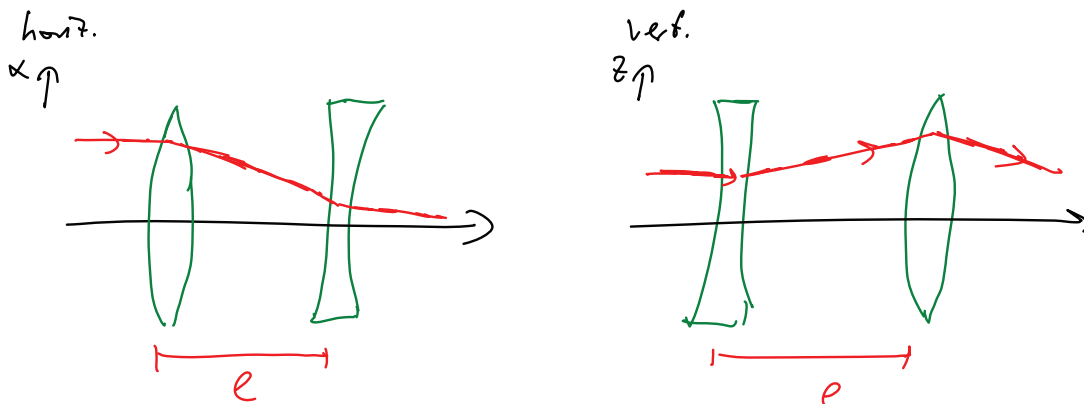
$\det \underline{M} = 1 \iff$ Liouville's Theorem
of phase space conservation

- simple Taylor expansion for small e/ρ (dipole)
or small $\sqrt{\eta} \ell$ (quadrupole) would not
fulfill $\det \underline{M} = 1$ \Downarrow



f₄) Quadrupole doublet:

focusing quadrupole + drift + defocusing quadrupole
 \Rightarrow both horizontal and vertical focusing
can be achieved!





\Rightarrow trajectories entering parallel to axis have larger amplitude in the focusing than in the defocusing lens \Rightarrow overall focusing
 \Rightarrow in thin lens approximation and $|f_1| = |f_2|$

$$\begin{aligned} \underline{M}_{2,x} &= \underline{M}_{2,x}^{\text{doublet}} = \underline{M}_{2,x}^{\text{def}} \underline{M}_{2,x}^{\text{dift}} \underline{M}_{2,x}^{\text{foc}} \\ &= \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix} \begin{pmatrix} 1 & e \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix} = \begin{pmatrix} 1 - e/f & e \\ -e/f^2 & 1 + e/f \end{pmatrix} \end{aligned}$$



Similar:

$$\underline{M}_{2,z}^{\text{doublet}} = \begin{pmatrix} 1 + e/f & e \\ -e/f^2 & 1 - e/f \end{pmatrix}$$

\Rightarrow focusing in both plans with overall refractive power: $M_{21} = C' = -e/f^2$

\Rightarrow effective focal length:

$$f_{\text{doublet}} = f^2/e$$



g) Accelerating Section

→ consider section of length l with $E_s = \text{const}$

⇒ for $\gamma \gg 1$

$$\frac{dp}{ds} = \frac{q}{c} E_s = \text{const}$$

⇒ momentum of particle

$$p(s) = p_0 + \frac{q}{c} E_s \cdot s$$

⇒ for transverse motion: ($u = x$ or z)

$$\frac{d}{ds} p_u = \frac{d}{ds} \left(\underbrace{\frac{p(s)}{c}}_{\approx \gamma m} v_u \right) = \frac{d}{ds} \left(\underbrace{p(s)}_{\substack{\uparrow \\ \text{not constant here!}}} \frac{du}{ds} \right) = 0$$



⇒ integrate: $p(s) \frac{du}{ds} = \text{const} = p_0 u_0'$

$$\Rightarrow \frac{du}{ds} = u'(s) = \frac{p_0 u_0'}{p_0 + \frac{q}{c} E_s \cdot s}$$

⇒ integrate:

$$u(s) = u_0 + u_0' \frac{c p_0}{q E_s} \ln \left(1 + \frac{q E_s}{c p_0} s \right)$$



=> for $s = l = \text{length of acc. section}$

with $\Delta p = \text{momentum gain} = \frac{q}{c} E_s l$

$$M_{\text{acc section}} = \begin{bmatrix} 1 & \frac{p_0}{\Delta p} l \ln\left(1 + \frac{\Delta p}{p_0}\right) & 0 & 0 \\ 0 & \frac{p_0}{p_0 + \Delta p} & 0 & 0 \\ 0 & 0 & 1 & \frac{p_0}{\Delta p} l \ln\left(1 + \frac{\Delta p}{p_0}\right) \\ 0 & 0 & 0 & \frac{p_0}{p_0 + \Delta p} \end{bmatrix}$$

Important: $\det M_{\text{acc section}} \neq 1$ (\Leftarrow) first order derivative term in eqn. of motion!



3.5 Momentum compaction factor:

$$x = G'(s) x_0 + S'(s) x_0' + D(s) \delta$$

=> dispersive trajectories $\Delta x_d = D(s) \delta$

=> change in path length $\Delta L_d = L_0 - L_d$

from before: $\Delta L_d = \delta \int_0^L \frac{1}{\beta(s)} D(s) ds$

$$= \delta I_d \propto \delta$$

=> define momentum compaction factor for circular accelerator:

$$\alpha = \frac{\Delta L_d / L_0}{\Delta p / p_0} = \frac{1}{L_0} \frac{\Delta L_d}{\delta} = \frac{1}{L_0} \int \frac{1}{\beta(s)} D(s) ds$$

\uparrow
length of ideal, closed orbit in circ. machine

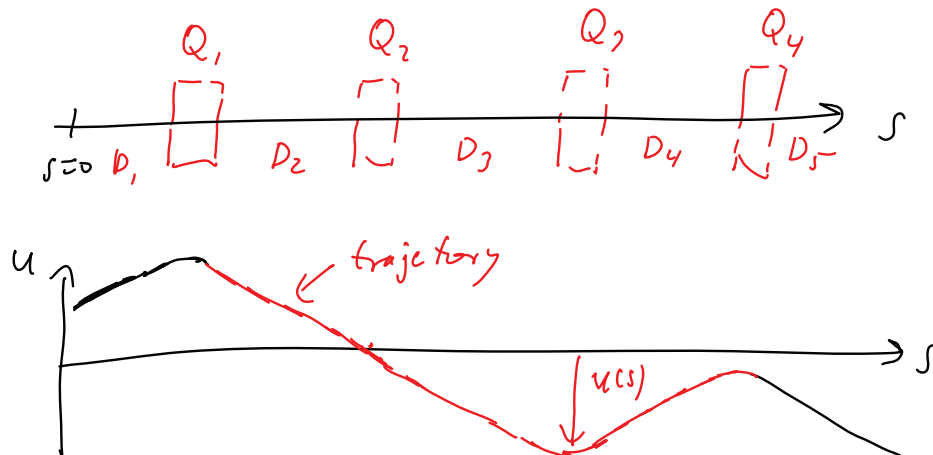


- $\Rightarrow \alpha \neq 0 \Rightarrow$ revolution period of particle depends on momentum
- \Rightarrow accelerating phase in RF cavity of particle depends on momentum error
- \Rightarrow Longitudinal phase focusing



3.6 Twiss Parameters: $\alpha, \beta, \gamma, \psi$

\Rightarrow for: Matrix formalism \rightarrow calculate individual particle trajectories through arbitrary structures of magnets





in the following: assume $\delta = 0$

equation of motion:

$$u'' + \mathcal{K}(s) u = 0$$

$$\Rightarrow \text{trajectory: } u(s) = C_1(s) u_0 + S_1(s) u_0'$$

\uparrow
for stable orbit: transverse
oscillation about the design orbit

= betatron oscillations



\Rightarrow oscillation amplitude and phase depend on the position s along the orbit

$$\Rightarrow \text{ansatz: } u(s) = \underbrace{\sqrt{2\gamma \beta(s)}}_{\text{position dependent amplitude of oscil.}} \sin(\psi(s) + \phi_0)$$

with γ and ϕ_0 defined by initial conditions

\Rightarrow insert into equ. of motion:

$$u'(s) = \sqrt{\frac{2\gamma}{\beta}} \left[\beta \psi' \cos(\psi(s) + \phi_0) - \alpha \sin(\psi(s) + \phi_0) \right]$$

$$\text{with } \boxed{\alpha(s) \equiv -\frac{1}{2} \beta'(s)}$$

note: $\alpha(s)$ is not the momentum compaction factor!



$$u''(s) = \sqrt{\frac{2\mathcal{J}}{\rho}} \left[(\beta\psi'' - 2\alpha\psi') \cos(\psi(s) + \phi_0) - \left(\alpha' + \frac{\alpha^2}{\rho} + \rho\psi'^2 \right) \sin(\psi(s) + \phi_0) \right]$$
$$= -\mathcal{K}u = \sqrt{\frac{2\mathcal{J}}{\rho}} \left[-\mathcal{K}\beta \sin(\psi(s) + \phi_0) \right]$$

\Rightarrow need:

$$\beta\psi'' - 2\alpha\psi' = 0 \quad (a)$$

$$\alpha' + \frac{\alpha^2}{\rho} + \rho\psi'^2 = \mathcal{K}\beta \quad (b)$$

\Rightarrow from (a): $\beta\psi'' - 2\alpha\psi' = \rho\psi'' + \rho'\psi' = (\beta\psi')' = 0$

integrate $\Rightarrow \psi' = \frac{I}{\beta} \Rightarrow \psi = \int_0^s \frac{I}{\beta(\tilde{s})} d\tilde{s}$



\Rightarrow from (b)

$$\alpha' + \gamma = \mathcal{K}\beta \quad \text{with } \gamma = \frac{I^2 + \alpha^2}{\rho}$$

\Rightarrow Universal choice for constant I : $I = 1$

\Rightarrow End result: Twiss parameters: $\alpha, \beta, \gamma, \psi$

$$\beta'(s) = -2\alpha(s)$$
$$\alpha'(s) = \mathcal{K}(s)\beta(s) - \gamma(s)$$
$$\gamma(s) = \frac{1 + \alpha^2}{\rho}$$
$$\psi(s) = \int_0^s \frac{1}{\beta(\tilde{s})} d\tilde{s}$$